

# Agilent ATF-551M4 Low Noise Enhancement Mode Pseudomorphic HEMT in a Miniature Leadless Package

## Data Sheet

### Description

Agilent Technologies' ATF-551M4 is a high dynamic range, super low noise, single supply E-pHEMT GAAs FET housed in a thin miniature leadless package.

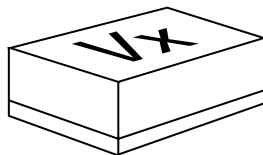
The combination of small device size, super low noise (under 1 dB Fmin from 2 to 6 GHz), high linearity and low power makes the ATF-551M4 ideal for LNA or hybrid module designs in wireless receiver in the 450 MHz to 10 GHz frequency band.

Applications include Cellular/PCS/ WCDMA handsets and data modem cards, fixed wireless infrastructure in the 2.4, 3.5 GHz and UNII frequency bands, as well as 2.4 GHz 802.11b, 5 GHz 802.11a and HIPERLAN/2 Wireless LAN PC-cards.

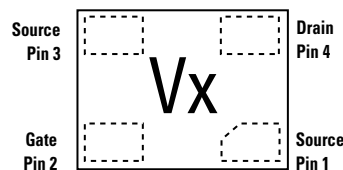
### Note:

1. Agilent's enhancement mode E-pHEMT devices are the first commercially available single-supply GaAs transistors that do not need a negative gate bias voltage for operation. They can help simplify the design and reduce the cost of receivers and transmitters in many applications in the 450 MHz to 10 GHz frequency range.

### MiniPak 1.4 mm x 1.2 mm Package



### Pin Connections and Package Marking



### Note:

Top View. Package marking provides orientation, product identification and date code.

"V" = Device Type Code

"x" = Date code character. A different character is assigned for each month and year.

### Features

- Very low noise figure and high linearity
- Single Supply Enhancement Mode Technology<sup>(1)</sup> optimized for 3V operation
- Excellent uniformity in product specifications
- 400 micron gate width
- Thin miniature package 1.4 mm x 1.2 mm x 0.7 mm
- Tape-and-reel packaging option available

### Specifications

- 2 GHz; 2.7V, 10 mA (typ.)
- 24.1 dBm output 3<sup>rd</sup> order intercept
- 14.6 dBm output power at 1 dB gain compression
- 0.5 dB noise figure
- 17.5 dB associated gain

### Applications

- Low Noise Amplifier for:
  - Cellular/PCS/WCDMA handsets and modem cards
  - 2.4 GHz, 3.5 GHz and UNII fixed wireless infrastructure
  - 2.4 GHz 802.11b Wireless LAN
  - 5 GHz 802.11a and HIPERLAN Wireless LAN
- General purpose discrete E-pHEMT for other ultra low noise applications



## ATF-551M4 Absolute Maximum Ratings<sup>[1]</sup>

Symbol	Parameter	Units	Absolute Maximum
$V_{DS}$	Drain-Source Voltage <sup>[2]</sup>	V	5
$V_{GS}$	Gate-Source Voltage <sup>[2]</sup>	V	-5 to 1
$V_{GD}$	Gate Drain Voltage <sup>[2]</sup>	V	-5 to 1
$I_{DS}$	Drain Current <sup>[2]</sup>	mA	100
$I_{GS}$	Gate Current <sup>[5]</sup>	mA	1
$P_{diss}$	Total Power Dissipation <sup>[3]</sup>	mW	270
$P_{in,max}$	RF Input Power	dBm	+10
$T_{CH}$	Channel Temperature	°C	150
$T_{STG}$	Storage Temperature	°C	-65 to 150
$\theta_{jc}$	Thermal Resistance <sup>[4]</sup>	°C/W	240

### Notes:

1. Operation of this device above any one of these parameters may cause permanent damage.
2. Assumes DC quiescent conditions.
3. Source lead temperature is 25°C. Derate 6 mW/°C for  $T_L > 40^\circ\text{C}$ .
4. Thermal resistance measured using 150°C Liquid Crystal Measurement method.
5. Device can safely handle +10 dBm RF Input Power provided  $I_{GS}$  is limited to 1 mA.  $I_{GS}$  at  $P_{1dB}$  drive RF level is bias circuit dependent. See applications section for additional information.

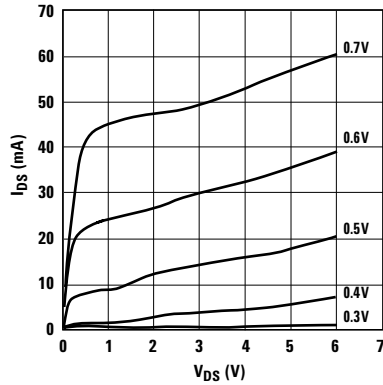


Figure 1. Typical I-V Curves.  
( $V_{GS} = 0.1\text{ V}$  per step)

## Product Consistency Distribution Charts<sup>[6]</sup>

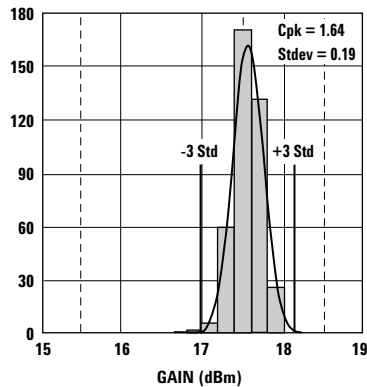


Figure 2. Capability Plot for Gain @ 2.7 V,  
10 mA. LSL = 15.5, Nominal = 17.5,  
USL = 18.5

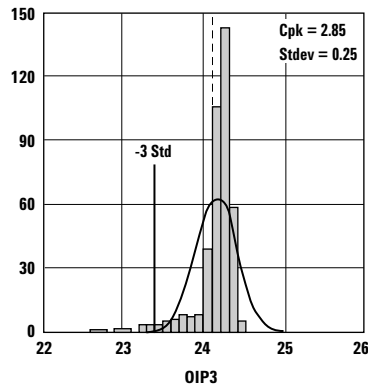


Figure 3. Capability Plot for OIP3 @ 2.7 V,  
10 mA. LSL = 22.0, Nominal = 24.1

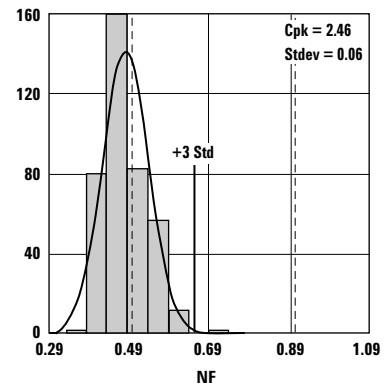


Figure 4. Capability Plot for NF @ 2.7 V,  
10 mA. Nominal = 0.5, USL = 0.9

### Note:

6. Distribution data sample size is 398 samples taken from 4 different wafers. Future wafers allocated to this product may have nominal values anywhere between the upper and lower limits. Measurements made on production test board. This circuit represents a trade-off between an optimal noise match and a realizable match based on production test equipment. Circuit losses have been de-embedded from actual measurements.

## ATF-551M4 Electrical Specifications

$T_A = 25^\circ\text{C}$ , RF parameters measured in a test circuit for a typical device

Symbol	Parameter and Test Condition		Units	Min.	Typ.	Max.	
Vgs	Operational Gate Voltage	Vds = 2.7V, Ids = 10 mA	V	0.3	0.47	0.65	
Vth	Threshold Voltage	Vds = 2.7V, Ids = 2 mA	V	0.18	0.37	0.53	
Idss	Saturated Drain Current	Vds = 2.7V, Vgs = 0V	$\mu\text{A}$	—	0.1	3	
Gm	Transconductance	Vds = 2.7V, gm = $\Delta\text{Idss}/\Delta\text{Vgs}$ ; $\Delta\text{Vgs} = 0.75 - 0.7 = 0.05\text{V}$	mmho	110	220	285	
Igss	Gate Leakage Current	Vgd = Vgs = -2.7V	$\mu\text{A}$	—	—	95	
NF	Noise Figure <sup>[1]</sup>	f = 2 GHz	Vds = 2.7V, Ids = 10 mA	dB	—	0.5	0.9
			Vds = 3V, Ids = 20 mA	dB	—	0.5	—
Gain	Gain <sup>[1]</sup>	f = 2 GHz	Vds = 2.7V, Ids = 10 mA	dB	15.5	17.5	18.5
			Vds = 3V, Ids = 20 mA	dB	—	18.0	—
OIP3	Output 3 <sup>rd</sup> Order Intercept Point <sup>[1]</sup>	f = 2 GHz	Vds = 2.7V, Ids = 10 mA	dBm	22	24.1	—
			Vds = 3V, Ids = 20 mA	dBm	—	30.0	—
P1dB	1dB Compressed Output Power <sup>[1]</sup>	f = 2 GHz	Vds = 2.7V, Ids = 10 mA	dBm	—	14.6	—
			Vds = 3V, Ids = 20 mA	dBm	—	16.0	—

### Notes:

- Measurements obtained using production test board described in Figure 5. Typical values were determined from a sample size of 398 parts from 4 wafers.

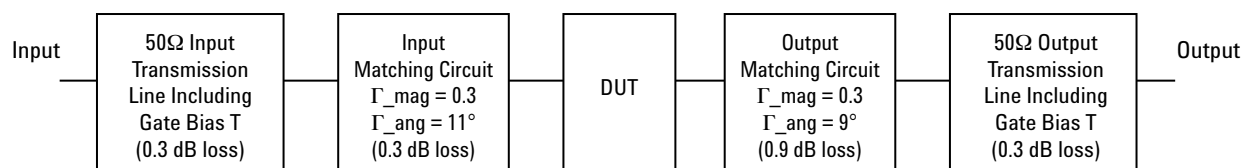


Figure 5. Block diagram of 2 GHz production test board used for Noise Figure, Gain, P1dB, OIP3, and IIP3 measurements. This circuit represents a trade-off between an optimal noise match, maximum OIP3 match and associated impedance matching circuit losses. Circuit losses have been de-embedded from actual measurements.

## ATF-551M4 Electrical Specifications (see notes 2 and 3, as indicated)

Symbol	Parameter and Test Condition		Units	Min.	Typ.	Max.	
Fmin	Minimum Noise Figure <sup>[2]</sup>	f = 900 GHz	Vds = 2.7V, Ids = 10 mA	dB	—	0.27	—
		f = 2 GHz	Vds = 2.7V, Ids = 10 mA	dB	—	0.41	—
		f = 3.9 GHz	Vds = 2.7V, Ids = 10 mA	dB	—	0.61	—
		f = 5.8 GHz	Vds = 2.7V, Ids = 10 mA	dB	—	0.88	—
Ga	Associated Gain <sup>[2]</sup>	f = 900 GHz	Vds = 2.7V, Ids = 10 mA	dB	—	21.8	—
		f = 2 GHz	Vds = 2.7V, Ids = 10 mA	dB	—	17.9	—
		f = 3.9 GHz	Vds = 2.7V, Ids = 10 mA	dB	—	14.2	—
		f = 5.8 GHz	Vds = 2.7V, Ids = 10 mA	dB	—	12.0	—
OIP3	Output 3 <sup>rd</sup> Order Intercept Point <sup>[3]</sup>	f = 900 GHz	Vds = 2.7V, Ids = 10 mA	dBm	—	22.1	—
		f = 3.9 GHz	Vds = 2.7V, Ids = 10 mA	dBm	—	24.3	—
		f = 5.8 GHz	Vds = 2.7V, Ids = 10 mA	dBm	—	24.5	—
P1dB	1dB Compressed Output Power <sup>[3]</sup>	f = 900 GHz	Vds = 2.7V, Ids = 10 mA	dBm	—	14.3	—
		f = 3.9 GHz	Vds = 2.7V, Ids = 10 mA	dBm	—	14.5	—
		f = 5.8 GHz	Vds = 2.7V, Ids = 10 mA	dBm	—	14.3	—

### Notes:

- The Fmin values are based on a set of 16 noise figure measurements made at 16 different impedances using an ATN NP5 test system. From these measurements Fmin is calculated. Refer to the noise parameter measurement section for more information.
- Measurements taken above and below 2 GHz was made using a double stub tuner at the input tuned for low noise and a double stub tuner at the output tuned for maximum OIP3. Circuit losses have been de-embedded from actual measurements.

## ATF-551M4 Typical Performance Curves

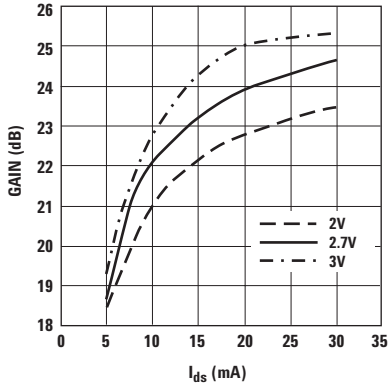


Figure 6. Gain vs.  $I_{ds}$  and  $V_{ds}$  at 900 MHz<sup>[1]</sup>.

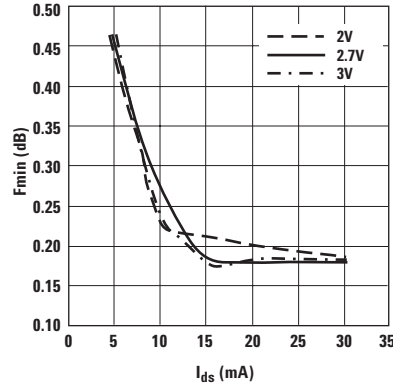


Figure 7.  $F_{min}$  vs.  $I_{ds}$  and  $V_{ds}$  at 900 MHz<sup>[2]</sup>.

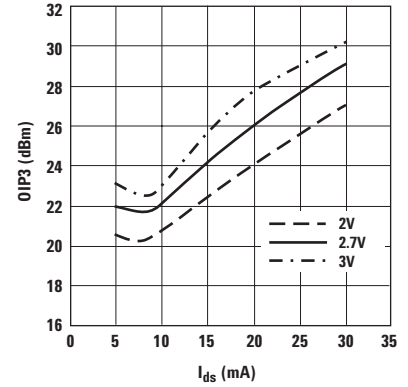


Figure 8. OIP3 vs.  $I_{ds}$  and  $V_{ds}$  at 900 MHz<sup>[1]</sup>.

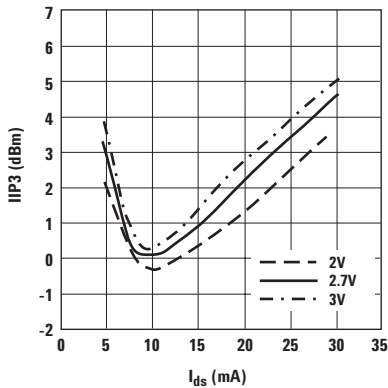


Figure 9. IIP3 vs.  $I_{ds}$  and  $V_{ds}$  at 900 MHz<sup>[1]</sup>.

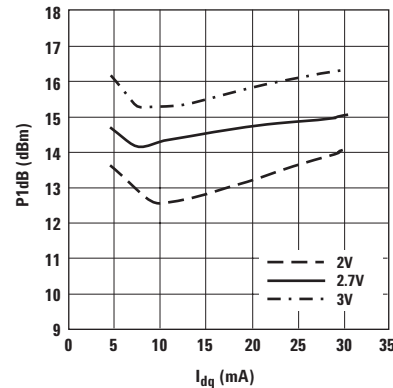
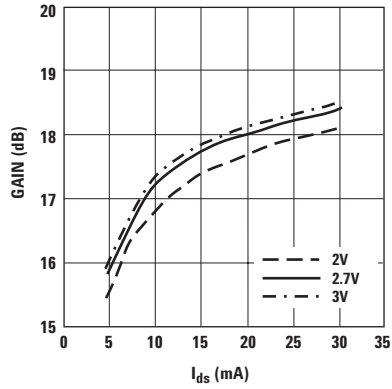


Figure 10. P1dB vs.  $I_{dq}$  and  $V_{ds}$  at 900 MHz<sup>[1]</sup>.

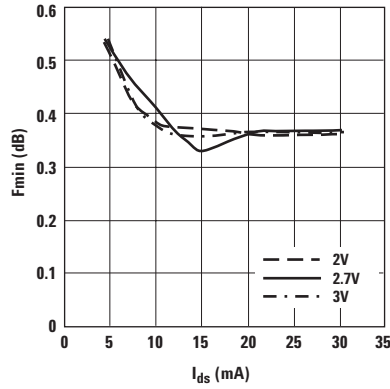
### Notes:

1. Measurements at 900MHz were made using an ICM fixture with a double stub tuner at the input tuned for low noise and a double stub tuner at the output tuned for maximum OIP3. Circuit losses have been de-embedded from actual measurements.
2. The  $F_{min}$  values are based on a set of 16 noise figure measurements made at 16 different impedances using an ATN NP5 test system. From these measurements  $F_{min}$  is calculated. Refer to the noise parameter measurement section for more information.
3. P1dB measurements are performed with passive biasing. Quiescent drain current,  $I_{dsq}$ , is set with zero RF drive applied. As P1dB is approached, the drain current may increase or point. At lower values of  $I_{dsq}$ , the device is running close to class B as power output approaches P1dB. This results in higher P1dB and higher PAE (power added efficiency) when compared to a device that is driven by a constant current source as is typically done with active biasing. As an example, at a  $V_{DS} = 2.7V$  and  $I_{dsq} = 5$  mA,  $I_d$  increases to 15 mA as a P1dB of +14.5 dBm is approached.

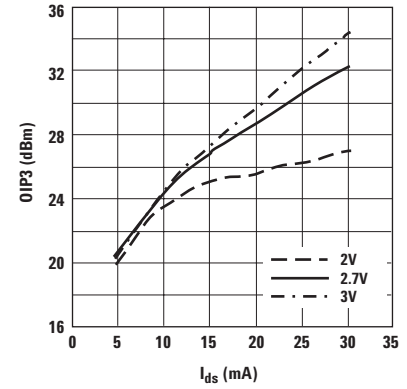
**ATF-551M4 Typical Performance Curves, continued**



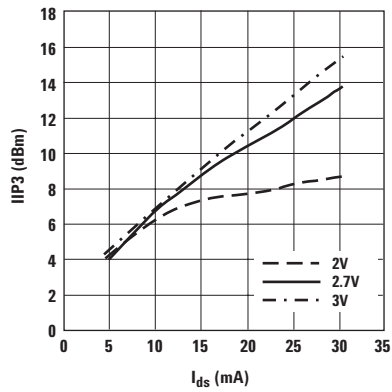
**Figure 11. Gain vs.  $I_{ds}$  and  $V_{ds}$  at 2 GHz<sup>[1]</sup>.**



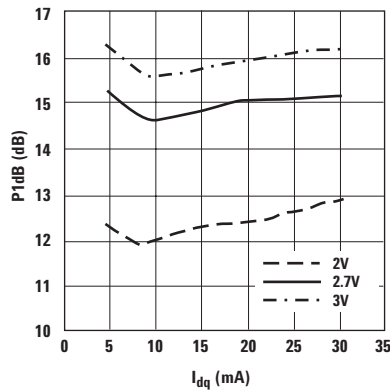
**Figure 12.  $F_{min}$  vs.  $I_{ds}$  and  $V_{ds}$  at 2 GHz<sup>[2]</sup>.**



**Figure 13. OIP3 vs.  $I_{ds}$  and  $V_{ds}$  at 2 GHz<sup>[1]</sup>.**



**Figure 14. IIP3 vs.  $I_{ds}$  and  $V_{ds}$  at 2 GHz<sup>[1]</sup>.**

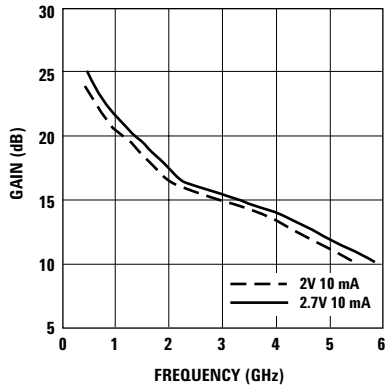


**Figure 15. P1dB vs.  $I_{dq}$  and  $V_{ds}$  at 2 GHz<sup>[1]</sup>.**

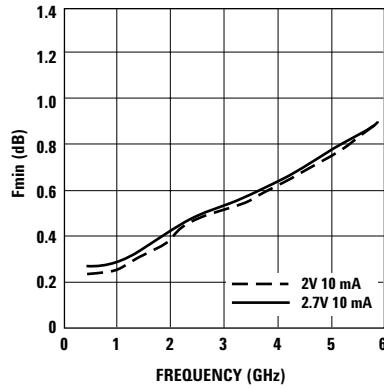
**Notes:**

1. Measurements at 2 GHz with biasing 2.7V, 10 mA were made on a fixed tuned production test board that was tuned for optimal OIP3 match with reasonable noise figure. This circuit represents a trade-off between optimal noise match, maximum OIP3 match and a realizable match based on production test board requirements. Measurements taken other than 2.7V, 10 mA biasing was made using a double stub tuner at the input tuned for low noise and a double stub tuner at the output tuned for maximum OIP3. Circuit losses have been de-embedded from actual measurements.
2. The  $F_{min}$  values are based on a set of 16 noise figure measurements made at 16 different impedances using an ATN NP5 test system. From these measurements  $F_{min}$  is calculated. Refer to the noise parameter measurement section for more information.
3. P1dB measurements are performed with passive biasing. Quiescent drain current,  $I_{dsq}$ , is set with zero RF drive applied. As P1dB is approached, the drain current may increase or point. At lower values of  $I_{dsq}$ , the device is running close to class B as power output approaches P1dB. This results in higher P1dB and higher PAE (power added efficiency) when compared to a device that is driven by a constant current source as is typically done with active biasing. As an example, at a  $V_{DS} = 2.7V$  and  $I_{dsq} = 5$  mA,  $I_d$  increases to 15 mA as a P1dB of +14.5 dBm is approached.

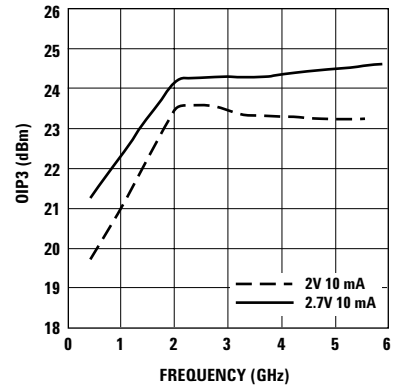
**ATF-551M4 Typical Performance Curves, continued**



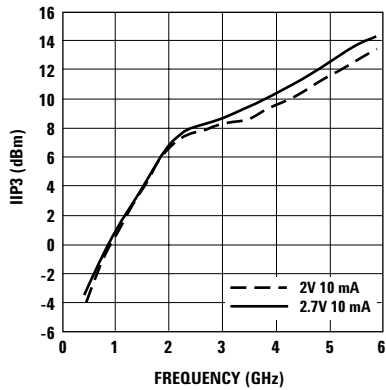
**Figure 16. Gain vs. Bias over Frequency<sup>[1]</sup>.**



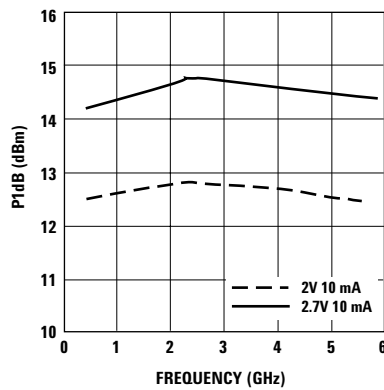
**Figure 17. Fmin vs. Bias over Frequency<sup>[2]</sup>.**



**Figure 18. OIP3 vs. Bias over Frequency<sup>[1]</sup>.**



**Figure 19. IIP3 vs. Bias over Frequency<sup>[1]</sup>.**

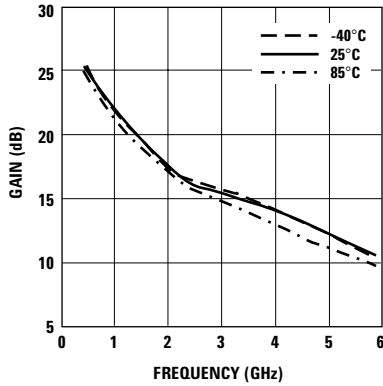


**Figure 20. P1dB vs. Bias over Frequency<sup>[1]</sup>.**

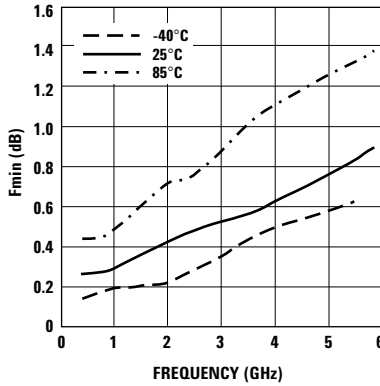
**Notes:**

1. Measurements at 2 GHz were made on a fixed tuned production test board that was tuned for optimal OIP3 match with reasonable noise figure at 2.7 V, 10 mA bias. This circuit represents a trade-off between optimal noise match, maximum OIP3 match and a realizable match based on production test board requirements. Measurements taken above and below 2 GHz was made using a double stub tuner at the input tuned for low noise and a double stub tuner at the output tuned for maximum OIP3. Circuit losses have been de-embedded from actual measurements.
2. The Fmin values are based on a set of 16 noise figure measurements made at 16 different impedances using an ATN NP5 test system. From these measurements Fmin is calculated. Refer to the noise parameter measurement section for more information.
3. P1dB measurements are performed with passive biasing. Quiescent drain current, Idsq, is set with zero RF drive applied. As P1dB is approached, the drain current may increase or point. At lower values of Idsq, the device is running close to class B as power output approaches P1dB. This results in higher P1dB and higher PAE (power added efficiency) when compared to a device that is driven by a constant current source as is typically done with active biasing. As an example, at a VDS = 2.7V and Idsq = 5 mA, Id increases to 15 mA as a P1dB of +14.5 dBm is approached.

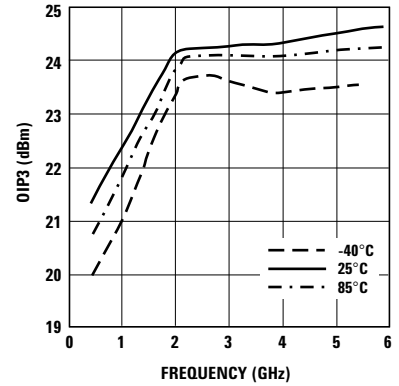
**ATF-551M4 Typical Performance Curves, continued**



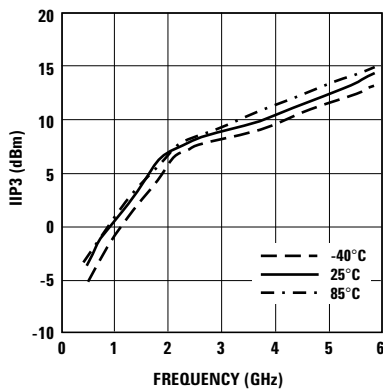
**Figure 21. Gain vs. Temperature and Frequency with Bias at 2.7V, 10 mA<sup>[1]</sup>.**



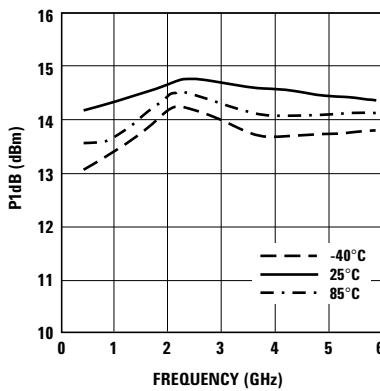
**Figure 22. Fmin vs. Temperature and Frequency with Bias at 2.7V, 10 mA<sup>[2]</sup>.**



**Figure 23. OIP3 vs. Temperature and Frequency with Bias at 2.7V, 10 mA<sup>[1]</sup>.**



**Figure 24. IIP3 vs. Temperature and Frequency with Bias at 2.7V, 10 mA<sup>[1]</sup>.**



**Figure 25. P1dB vs. Temperature and Frequency with Bias at 2.7V, 10 mA<sup>[1]</sup>.**

**Notes:**

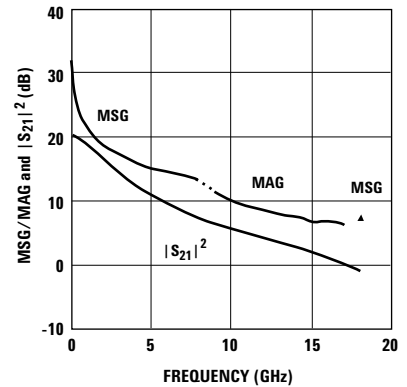
1. Measurements at 2 GHz were made on a fixed tuned production test board that was tuned for optimal OIP3 match with reasonable noise figure at 2.7 V, 10 mA bias. This circuit represents a trade-off between optimal noise match, maximum OIP3 match and a realizable match based on production test board requirements. Measurements taken above and below 2 GHz was made using a double stub tuner at the input tuned for low noise and a double stub tuner at the output tuned for maximum OIP3. Circuit losses have been de-embedded from actual measurements.
2. The Fmin values are based on a set of 16 noise figure measurements made at 16 different impedances using an ATN NP5 test system. From these measurements Fmin is calculated. Refer to the noise parameter measurement section for more information.
3. P1dB measurements are performed with passive biasing. Quiescent drain current, Idsq, is set with zero RF drive applied. As P1dB is approached, the drain current may increase or point. At lower values of Idsq, the device is running close to class B as power output approaches P1dB. This results in higher P1dB and higher PAE (power added efficiency) when compared to a device that is driven by a constant current source as is typically done with active biasing. As an example, at a VDS = 2.7V and Idsq = 5 mA, Id increases to 15 mA as a P1dB of +14.5 dBm is approached.

**ATF-551M4 Typical Scattering Parameters,  $V_{DS} = 2V, I_{DS} = 10\text{ mA}$**

Freq. GHz	$S_{11}$			$S_{21}$		$S_{12}$		$S_{22}$		MSG/MAG dB
	Mag.	Ang.	dB	Mag.	Ang.	Mag.	Ang.	Mag.	Ang.	
0.1	0.995	-6.0	20.41	10.479	175.9	0.007	86.3	0.803	-3.3	31.75
0.5	0.954	-29.1	19.95	9.946	158.2	0.031	71.6	0.758	-15.6	25.06
0.9	0.906	-50.7	19.35	9.280	144.2	0.052	60.8	0.710	-27.4	22.52
1.0	0.896	-55.7	19.18	9.103	141.0	0.056	58.3	0.692	-30.2	22.11
1.5	0.833	-79.5	18.15	8.080	125.6	0.075	46.8	0.611	-42.3	20.32
1.9	0.790	-96.5	17.22	7.260	114.9	0.085	39.0	0.547	-50.4	19.32
2.0	0.781	-100.4	17.00	7.078	112.5	0.087	37.3	0.532	-52.3	19.10
2.5	0.739	-118.5	15.84	6.197	101.1	0.095	29.8	0.463	-60.6	18.14
3.0	0.710	-134.4	14.74	5.459	91.2	0.099	23.7	0.404	-67.6	17.41
4.0	0.683	-160.0	12.75	4.341	74.5	0.104	14.8	0.318	-79.6	16.21
5.0	0.679	-179.8	11.03	3.559	60.3	0.105	8.6	0.263	-91.2	15.30
6.0	0.680	166.5	9.65	3.036	48.5	0.107	5.0	0.220	-99.5	14.53
7.0	0.681	154.0	8.43	2.638	37.2	0.107	2.1	0.199	-111.0	13.92
8.0	0.683	143.7	7.43	2.353	26.4	0.110	-0.3	0.185	-123.4	13.30
9.0	0.690	132.7	6.53	2.122	15.7	0.113	-2.6	0.181	-137.7	11.27
10.0	0.687	119.7	5.72	1.932	4.5	0.117	-5.4	0.185	-151.1	9.97
11.0	0.691	106.5	4.98	1.775	-6.4	0.122	-8.4	0.196	-163.5	9.14
12.0	0.696	92.6	4.28	1.636	-17.7	0.129	-12.3	0.209	-174.4	8.44
13.0	0.713	81.8	3.53	1.501	-28.6	0.135	-16.2	0.206	171.4	7.80
14.0	0.747	67.4	2.82	1.384	-40.4	0.143	-21.8	0.211	151.2	7.62
15.0	0.759	55.5	1.97	1.255	-51.8	0.149	-27.4	0.237	131.8	6.73
16.0	0.808	45.4	1.00	1.122	-62.4	0.153	-33.3	0.269	113.3	6.90
17.0	0.828	37.3	-0.01	0.999	-72.7	0.157	-39.2	0.322	95.4	6.20
18.0	0.870	30.9	-1.04	0.887	-82.6	0.159	-45.2	0.383	80.1	7.47

**Typical Noise Parameters,  $V_{DS} = 2V, I_{DS} = 10\text{ mA}$**

Freq GHz	$F_{min}$ dB	$\Gamma_{opt}$ Mag.	$\Gamma_{opt}$ Ang.	$R_n/50$	$G_a$ dB
0.5	0.24	0.62	-4.3	0.14	23.50
0.9	0.24	0.56	8.8	0.13	21.66
1.0	0.28	0.52	13.5	0.12	21.61
1.9	0.45	0.47	38.6	0.11	18.04
2.0	0.39	0.47	42.9	0.11	17.88
2.4	0.47	0.42	52.8	0.11	16.76
3.0	0.55	0.35	74.0	0.09	15.66
3.9	0.61	0.32	105.4	0.08	14.10
5.0	0.74	0.33	144.0	0.06	12.74
5.8	0.89	0.36	164.3	0.05	11.83
6.0	0.90	0.37	166.1	0.05	11.63
7.0	1.03	0.38	-170.9	0.06	10.71
8.0	1.13	0.44	-157.2	0.07	9.99
9.0	1.27	0.48	-142.4	0.09	9.36
10.0	1.53	0.46	-126.0	0.17	8.46



**Figure 26. MSG/MAG and  $|S_{21}|^2$  vs. Frequency at 2V, 10 mA.**

**Notes:**

1. The  $F_{min}$  values are based on a set of 16 noise figure measurements made at 16 different impedances using an ATN NP5 test system. From these measurements  $F_{min}$  is calculated. Refer to the noise parameter measurement section for more information.
2. S and noise parameters are measured on a microstrip line made on 0.010 inch thick alumina carrier assembly. The input reference plane is at the end of the gate pad. The output reference plane is at the end of the drain pad.

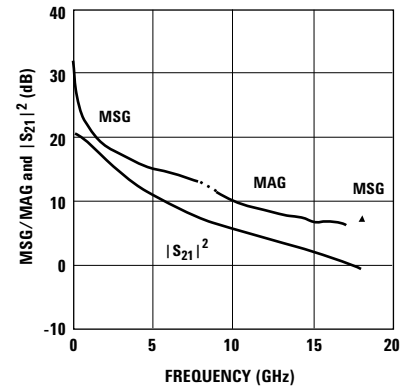


**ATF-551M4 Typical Scattering Parameters,  $V_{DS} = 2V, I_{DS} = 15\text{ mA}$**

Freq. GHz	$S_{11}$			$S_{21}$			$S_{12}$		$S_{22}$		MSG/MAG dB
	Mag.	Ang.	dB	Mag.	Ang.	Mag.	Ang.	Mag.	Ang.		
0.1	0.995	-6.6	21.93	12.489	175.5	0.006	86.2	0.765	-3.7	33.18	
0.5	0.947	-31.6	21.41	11.757	156.7	0.029	70.9	0.715	-17.0	26.08	
0.9	0.892	-54.7	20.67	10.804	142.0	0.048	59.7	0.659	-29.6	23.52	
1.0	0.880	-60.1	20.46	10.547	138.6	0.052	57.1	0.641	-32.5	23.07	
1.5	0.812	-84.9	19.26	9.186	123.0	0.067	46.0	0.555	-45.0	21.37	
1.9	0.768	-102.1	18.23	8.153	112.3	0.076	38.7	0.489	-53.1	20.31	
2.0	0.758	-106.1	17.98	7.923	109.9	0.077	37.2	0.474	-55.0	20.12	
2.5	0.718	-124.1	16.73	6.859	98.9	0.084	30.5	0.407	-63.2	19.12	
3.0	0.692	-139.7	15.55	5.991	89.3	0.088	25.3	0.352	-70.2	18.33	
4.0	0.671	-164.5	13.47	4.716	73.3	0.092	18.0	0.272	-82.3	17.10	
5.0	0.670	176.6	11.70	3.845	59.7	0.095	13.1	0.222	-94.5	16.07	
6.0	0.671	163.5	10.30	3.273	48.3	0.098	10.5	0.181	-103.2	15.24	
7.0	0.674	151.5	9.06	2.838	37.4	0.101	8.2	0.164	-115.4	14.49	
8.0	0.676	141.6	8.06	2.528	27.0	0.105	6.1	0.152	-128.5	12.66	
9.0	0.684	130.9	7.14	2.276	16.5	0.111	3.7	0.150	-143.3	11.51	
10.0	0.682	118.0	6.33	2.072	5.6	0.117	0.6	0.156	-156.9	10.35	
11.0	0.686	105.1	5.59	1.903	-5.0	0.124	-3.1	0.170	-169.0	9.57	
12.0	0.691	91.4	4.88	1.753	-16.1	0.132	-7.6	0.183	-179.3	8.87	
13.0	0.708	80.9	4.13	1.609	-26.9	0.140	-12.3	0.181	165.9	8.27	
14.0	0.744	66.5	3.42	1.483	-38.5	0.148	-18.6	0.188	145.0	8.14	
15.0	0.756	54.9	2.59	1.347	-49.7	0.155	-24.9	0.217	125.0	7.23	
16.0	0.805	45.0	1.59	1.201	-60.2	0.158	-31.2	0.253	106.8	7.38	
17.0	0.825	37.0	0.61	1.073	-70.4	0.161	-37.5	0.310	89.4	6.61	
18.0	0.870	30.7	-0.41	0.954	-80.1	0.163	-43.8	0.373	74.9	7.67	

**Typical Noise Parameters,  $V_{DS} = 2V, I_{DS} = 15\text{ mA}$**

Freq GHz	$F_{min}$ dB	$\Gamma_{opt}$ Mag.	$\Gamma_{opt}$ Ang.	$R_n/50$	$G_a$ dB
0.5	0.21	0.61	-6.1	0.12	24.12
0.9	0.21	0.55	7.0	0.12	22.18
1.0	0.27	0.50	11.4	0.11	22.12
1.9	0.42	0.46	38.1	0.10	18.61
2.0	0.37	0.43	42.7	0.10	18.52
2.4	0.44	0.39	52.9	0.10	17.34
3.0	0.52	0.32	74.4	0.08	16.21
3.9	0.57	0.28	108.3	0.07	14.65
5.0	0.71	0.30	149.5	0.06	13.27
5.8	0.85	0.35	170.0	0.05	12.38
6.0	0.86	0.35	171.7	0.05	12.19
7.0	0.97	0.38	-165.9	0.06	11.24
8.0	1.08	0.43	-152.1	0.07	10.49
9.0	1.22	0.47	-138.1	0.10	9.84
10.0	1.44	0.46	-122.5	0.17	8.96



**Figure 27. MSG/MAG and  $|S_{21}|^2$  vs. Frequency at 2V, 15 mA.**

**Notes:**

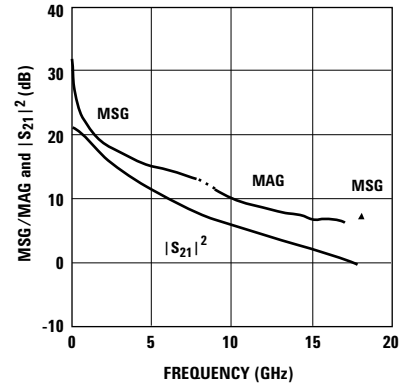
1. The  $F_{min}$  values are based on a set of 16 noise figure measurements made at 16 different impedances using an ATN NP5 test system. From these measurements  $F_{min}$  is calculated. Refer to the noise parameter measurement section for more information.
2. S and noise parameters are measured on a microstrip line made on 0.010 inch thick alumina carrier assembly. The input reference plane is at the end of the gate pad. The output reference plane is at the end of the drain pad.

**ATF-551M4 Typical Scattering Parameters,  $V_{DS} = 2V, I_{DS} = 20\text{ mA}$**

Freq. GHz	$S_{11}$			$S_{21}$			$S_{12}$		$S_{22}$		MSG/MAG dB
	Mag.	Ang.	dB	Mag.	Ang.	Mag.	Ang.	Mag.	Ang.		
0.1	0.994	-6.9	22.85	13.876	175.3	0.006	85.6	0.740	-3.9	33.64	
0.5	0.942	-33.3	22.27	12.985	155.7	0.027	70.4	0.687	-17.8	26.82	
0.9	0.882	-57.3	21.44	11.806	140.5	0.045	59.0	0.627	-30.9	24.19	
1.0	0.869	-62.8	21.21	11.491	137.1	0.048	56.5	0.608	-33.8	23.79	
1.5	0.798	-88.1	19.90	9.881	121.3	0.062	45.7	0.520	-46.4	22.02	
1.9	0.753	-105.5	18.79	8.704	110.7	0.070	38.9	0.455	-54.4	20.95	
2.0	0.744	-109.5	18.53	8.443	108.4	0.071	37.4	0.441	-56.3	20.75	
2.5	0.706	-127.4	17.22	7.262	97.5	0.077	31.3	0.376	-64.3	19.75	
3.0	0.681	-142.7	16.01	6.314	88.2	0.081	26.7	0.323	-71.0	18.92	
4.0	0.663	-167.0	13.88	4.943	72.5	0.085	20.3	0.248	-82.9	17.65	
5.0	0.664	174.6	12.09	4.021	59.3	0.089	16.2	0.201	-95.2	16.55	
6.0	0.666	161.9	10.68	3.418	48.1	0.093	14.1	0.162	-103.7	15.65	
7.0	0.670	150.1	9.43	2.962	37.3	0.097	12.0	0.144	-116.4	14.85	
8.0	0.673	140.4	8.42	2.637	27.1	0.103	10.0	0.133	-130.0	12.78	
9.0	0.681	129.8	7.51	2.373	16.8	0.109	7.4	0.131	-145.9	11.65	
10.0	0.678	117.1	6.68	2.158	6.0	0.117	3.7	0.139	-160.3	10.56	
11.0	0.682	104.3	5.94	1.982	-4.6	0.125	-0.2	0.154	-172.7	9.80	
12.0	0.688	90.6	5.23	1.826	-15.6	0.133	-5.2	0.168	176.9	9.11	
13.0	0.706	80.3	4.48	1.675	-26.3	0.142	-10.3	0.169	161.6	8.56	
14.0	0.743	65.9	3.76	1.542	-38.0	0.150	-17.0	0.182	139.6	8.46	
15.0	0.753	54.4	2.92	1.400	-48.9	0.157	-23.6	0.212	121.2	7.48	
16.0	0.804	44.7	1.93	1.249	-59.3	0.160	-30.1	0.250	103.8	7.76	
17.0	0.824	36.7	0.95	1.116	-69.4	0.163	-36.5	0.306	87.0	6.93	
18.0	0.869	30.6	-0.05	0.994	-78.9	0.165	-43.0	0.367	73.0	7.80	

**Typical Noise Parameters,  $V_{DS} = 2V, I_{DS} = 20\text{ mA}$**

Freq GHz	$F_{min}$ dB	$\Gamma_{opt}$ Mag.	$\Gamma_{opt}$ Ang.	$R_{n/50}$	$G_a$ dB
0.5	0.19	0.59	-7.0	0.11	23.50
0.9	0.20	0.54	6.3	0.11	21.66
1.0	0.25	0.48	10.1	0.10	21.61
1.9	0.41	0.43	38.7	0.09	18.04
2.0	0.36	0.41	43.1	0.09	17.88
2.4	0.43	0.37	53.4	0.09	16.76
3.0	0.51	0.29	76.3	0.08	15.66
3.9	0.58	0.26	112.7	0.07	14.10
5.0	0.70	0.29	154.0	0.05	12.74
5.8	0.85	0.34	173.6	0.05	11.83
6.0	0.86	0.35	175.9	0.05	11.63
7.0	0.94	0.37	-162.3	0.06	10.71
8.0	1.07	0.42	-148.2	0.08	9.99
9.0	1.20	0.48	-135.2	0.10	9.36
10.0	1.43	0.46	-119.5	0.17	8.46



**Figure 28. MSG/MAG and  $|S_{21}|^2$  vs. Frequency at 2V, 20 mA.**

**Notes:**

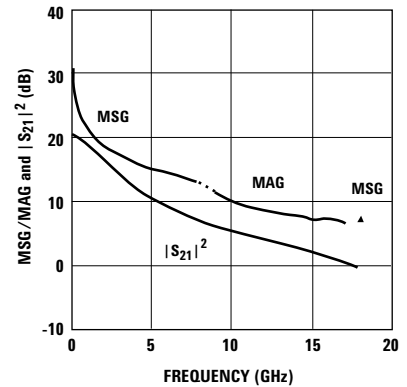
1. The  $F_{min}$  values are based on a set of 16 noise figure measurements made at 16 different impedances using an ATN NP5 test system. From these measurements  $F_{min}$  is calculated. Refer to the noise parameter measurement section for more information.
2. S and noise parameters are measured on a microstrip line made on 0.010 inch thick alumina carrier assembly. The input reference plane is at the end of the gate pad. The output reference plane is at the end of the drain pad.

**ATF-551M4 Typical Scattering Parameters,  $V_{DS} = 2.7V$ ,  $I_{DS} = 10\text{ mA}$**

Freq. GHz	$S_{11}$			$S_{21}$			$S_{12}$		$S_{22}$		MSG/MAG dB
	Mag.	Ang.	dB	Mag.	Ang.	Mag.	Ang.	Mag.	Ang.		
0.1	0.995	-5.9	20.55	10.656	175.9	0.006	86.3	0.825	-3.0	32.49	
0.5	0.955	-28.7	20.11	10.129	158.4	0.028	72.0	0.782	-14.0	25.58	
0.9	0.907	-50.0	19.52	9.466	144.6	0.046	61.3	0.735	-24.5	23.13	
1.0	0.896	-55.0	19.36	9.292	141.4	0.050	58.8	0.717	-27.0	22.69	
1.5	0.833	-78.6	18.34	8.265	126.1	0.067	47.6	0.639	-37.6	20.91	
1.9	0.789	-95.5	17.43	7.439	115.4	0.076	40.0	0.577	-44.6	19.91	
2.0	0.779	-99.4	17.21	7.255	113.0	0.078	38.4	0.562	-46.2	19.69	
2.5	0.737	-117.4	16.07	6.361	101.7	0.085	31.0	0.495	-53.1	18.74	
3.0	0.707	-133.4	14.98	5.610	91.8	0.089	25.1	0.439	-58.8	18.00	
4.0	0.679	-159.1	13.01	4.471	75.0	0.093	16.6	0.357	-68.3	16.82	
5.0	0.674	-178.9	11.30	3.673	60.8	0.094	10.9	0.303	-77.6	15.92	
6.0	0.675	167.3	9.93	3.136	49.1	0.095	8.1	0.264	-83.7	15.19	
7.0	0.676	154.9	8.72	2.728	37.7	0.096	5.9	0.244	-93.5	14.54	
8.0	0.679	144.5	7.73	2.435	27.0	0.099	4.3	0.230	-104.1	12.94	
9.0	0.686	133.5	6.84	2.198	16.2	0.102	2.9	0.222	-116.6	11.58	
10.0	0.684	120.8	6.03	2.002	5.1	0.107	0.7	0.222	-129.0	10.44	
11.0	0.688	107.5	5.30	1.841	-5.9	0.113	-1.7	0.230	-140.8	9.69	
12.0	0.693	93.7	4.59	1.696	-17.2	0.121	-5.2	0.239	-151.9	9.02	
13.0	0.710	82.7	3.86	1.559	-28.2	0.129	-8.9	0.232	-164.6	8.47	
14.0	0.743	68.6	3.19	1.443	-39.8	0.139	-14.3	0.222	-176.6	8.42	
15.0	0.760	56.5	2.37	1.314	-51.5	0.147	-20.2	0.232	-155.6	7.69	
16.0	0.805	46.2	1.42	1.177	-62.2	0.153	-26.2	0.251	-134.3	8.26	
17.0	0.830	38.1	0.43	1.051	-72.8	0.158	-32.5	0.293	-112.0	8.07	
18.0	0.872	31.5	-0.58	0.935	-83.1	0.163	-39.1	0.353	-92.7	7.59	

**Typical Noise Parameters,  $V_{DS} = 2.7V$ ,  $I_{DS} = 10\text{ mA}$**

Freq GHz	$F_{min}$ dB	$\Gamma_{opt}$ Mag.	$\Gamma_{opt}$ Ang.	$R_n/50$	$G_a$ dB
0.5	0.26	0.64	-4.4	0.14	23.79
0.9	0.27	0.57	7.5	0.13	21.80
1.0	0.30	0.54	11.1	0.13	21.60
1.9	0.46	0.49	36.6	0.11	18.06
2.0	0.41	0.48	40.4	0.12	17.92
2.4	0.47	0.44	50.3	0.11	16.79
3.0	0.55	0.36	69.5	0.10	15.70
3.9	0.61	0.32	101.3	0.08	14.24
5.0	0.74	0.32	139.5	0.06	12.86
5.8	0.88	0.35	161.5	0.05	12.01
6.0	0.90	0.35	163.9	0.05	11.82
7.0	1.00	0.37	-173.6	0.06	10.93
8.0	1.12	0.41	-158.2	0.07	10.24
9.0	1.25	0.46	-143.0	0.09	9.66
10.0	1.46	0.46	-127.2	0.15	8.85



**Figure 29. MSG/MAG and  $|S_{21}|^2$  vs. Frequency at 2.7V, 10 mA.**

**Notes:**

1. The  $F_{min}$  values are based on a set of 16 noise figure measurements made at 16 different impedances using an ATN NP5 test system. From these measurements  $F_{min}$  is calculated. Refer to the noise parameter measurement section for more information.
2. S and noise parameters are measured on a microstrip line made on 0.010 inch thick alumina carrier assembly. The input reference plane is at the end of the gate pad. The output reference plane is at the end of the drain pad.

**ATF-551M4 Typical Scattering Parameters,  $V_{DS} = 2.7V$ ,  $I_{DS} = 15\text{ mA}$**

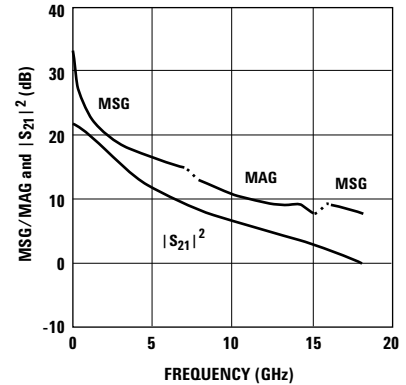
Freq. GHz	$S_{11}$			$S_{21}$		$S_{12}$		$S_{22}$		MSG/MAG dB
	Mag.	Ang.	dB	Mag.	Ang.	Mag.	Ang.	Mag.	Ang.	
0.1	0.995	-6.5	21.98	12.559	175.6	0.006	86.4	0.793	-3.2	33.21
0.5	0.949	-31.2	21.47	11.839	156.9	0.026	71.0	0.745	-15.2	26.58
0.9	0.894	-54.0	20.75	10.905	142.3	0.043	60.1	0.691	-26.4	24.04
1.0	0.882	-59.4	20.55	10.650	138.9	0.047	57.5	0.673	-28.9	23.55
1.5	0.814	-84.0	19.37	9.298	123.4	0.061	46.6	0.589	-39.7	21.83
1.9	0.768	-101.1	18.34	8.265	112.7	0.068	39.5	0.526	-46.6	20.85
2.0	0.758	-105.1	18.10	8.034	110.3	0.070	38.0	0.511	-48.1	20.60
2.5	0.718	-123.1	16.86	6.966	99.3	0.076	31.4	0.447	-54.6	19.62
3.0	0.691	-138.7	15.70	6.095	89.7	0.079	26.3	0.393	-59.9	18.87
4.0	0.668	-163.5	13.64	4.806	73.6	0.083	19.4	0.318	-68.8	17.63
5.0	0.667	177.5	11.88	3.928	59.9	0.085	15.0	0.268	-77.7	16.65
6.0	0.668	164.3	10.49	3.345	48.5	0.088	13.1	0.230	-83.3	15.80
7.0	0.671	152.2	9.26	2.904	37.5	0.091	11.4	0.212	-93.0	15.04
8.0	0.673	142.3	8.27	2.591	27.0	0.095	10.0	0.198	-103.4	12.89
9.0	0.682	131.6	7.37	2.335	16.4	0.101	8.4	0.190	-116.2	11.88
10.0	0.677	118.5	6.56	2.128	5.4	0.107	5.6	0.190	-129.6	10.70
11.0	0.684	105.8	5.83	1.956	-5.3	0.115	2.6	0.198	-142.6	10.06
12.0	0.690	91.7	5.12	1.804	-16.7	0.124	-1.7	0.210	-154.2	9.46
13.0	0.707	81.2	4.38	1.656	-27.5	0.133	-6.1	0.205	-167.8	8.93
14.0	0.744	66.4	3.68	1.528	-39.4	0.143	-12.3	0.200	-172.5	9.10
15.0	0.750	55.1	2.85	1.389	-50.6	0.151	-18.7	0.212	-150.9	7.85
16.0	0.806	45.2	1.88	1.242	-61.2	0.156	-25.1	0.236	129.7	9.01
17.0	0.824	37.1	0.92	1.112	-71.5	0.162	-31.6	0.282	107.9	8.37
18.0	0.872	31.0	-0.08	0.991	-81.5	0.166	-38.2	0.337	89.7	7.76

**Typical Noise Parameters,  $V_{DS} = 2.7V$ ,  $I_{DS} = 15\text{ mA}$**

Freq GHz	$F_{min}$	$\Gamma_{opt}$	$\Gamma_{opt}$	$R_{n/50}$	$G_a$
	dB	Mag.	Ang.		
0.5	0.18	0.61	-6.0	0.12	24.49
0.9	0.18	0.56	6.8	0.12	22.38
1.0	0.24	0.5	10.7	0.11	22.32
1.9	0.38	0.45	36.9	0.1	18.78
2.0	0.33	0.43	41.9	0.1	18.65
2.4	0.42	0.39	50.9	0.1	17.47
3.0	0.5	0.31	73.0	0.08	16.37
3.9	0.55	0.28	107.0	0.07	14.83
5.0	0.66	0.29	146.6	0.06	13.4
5.8	0.83	0.33	168.7	0.05	12.54
6.0	0.84	0.34	170.7	0.05	12.36
7.0	0.95	0.36	-166.9	0.06	11.44
8.0	1.06	0.41	-152.3	0.07	10.69
9.0	1.18	0.46	-138.1	0.1	10.12
10.0	1.43	0.44	-122.5	0.16	9.21

**Notes:**

- The  $F_{min}$  values are based on a set of 16 noise figure measurements made at 16 different impedances using an ATN NP5 test system. From these measurements  $F_{min}$  is calculated. Refer to the noise parameter measurement section for more information.
- S and noise parameters are measured on a microstrip line made on 0.010 inch thick alumina carrier assembly. The input reference plane is at the end of the gate pad. The output reference plane is at the end of the drain pad.



**Figure 30. MSG/MAG and  $|S_{21}|^2$  vs. Frequency at 2.7V, 15 mA.**

**ATF-551M4 Typical Scattering Parameters,  $V_{DS} = 2.7V$ ,  $I_{DS} = 20\text{ mA}$**

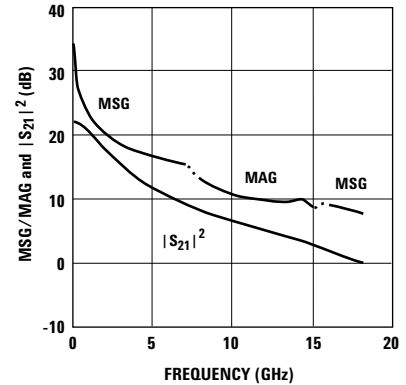
Freq. GHz	$S_{11}$			$S_{21}$			$S_{12}$		$S_{22}$		MSG/MAG dB
	Mag.	Ang.	dB	Mag.	Ang.	Mag.	Ang.	Mag.	Ang.		
0.1	0.995	-6.8	22.92	13.988	175.4	0.005	86.4	0.772	-3.4	34.47	
0.5	0.943	-33.0	22.35	13.103	155.9	0.024	70.6	0.72	-15.7	27.37	
0.9	0.883	-56.9	21.53	11.932	140.7	0.04	59.4	0.662	-27.1	24.75	
1.0	0.87	-62.4	21.30	11.616	137.3	0.043	56.9	0.643	-29.6	24.32	
1.5	0.798	-87.6	20.00	10.004	121.6	0.056	46.2	0.557	-40.2	22.52	
1.9	0.752	-104.9	18.91	8.822	111.0	0.063	39.6	0.494	-46.7	21.46	
2.0	0.743	-108.8	18.65	8.557	108.6	0.064	38.2	0.48	-48.1	21.26	
2.5	0.704	-126.7	17.35	7.367	97.8	0.069	32.3	0.417	-54.2	20.28	
3.0	0.68	-142.1	16.14	6.411	88.4	0.072	27.8	0.367	-59.0	19.50	
4.0	0.66	-166.3	14.02	5.026	72.8	0.076	22.0	0.297	-67.2	18.20	
5.0	0.662	175.2	12.25	4.095	59.5	0.079	18.6	0.251	-75.7	17.15	
6.0	0.664	162.6	10.84	3.483	48.4	0.083	17.4	0.216	-80.7	16.23	
7.0	0.667	150.9	9.61	3.022	37.6	0.087	16.1	0.199	-90.4	14.69	
8.0	0.67	141.2	8.61	2.695	27.3	0.093	14.8	0.185	-100.6	13.08	
9.0	0.679	130.8	7.71	2.429	16.9	0.099	13.0	0.177	-113.5	12.08	
10.0	0.677	118.1	6.90	2.213	6.0	0.107	9.9	0.178	-127.2	11.08	
11.0	0.683	105.4	6.17	2.034	-4.6	0.116	6.4	0.186	-140.4	10.44	
12.0	0.688	91.4	5.46	1.876	-15.8	0.126	1.8	0.198	-152.2	9.85	
13.0	0.705	80.9	4.72	1.722	-26.5	0.136	-3.2	0.193	-165.9	9.37	
14.0	0.741	66.5	4.03	1.59	-38.3	0.146	-9.8	0.188	173.7	9.78	
15.0	0.75	55.0	3.19	1.444	-49.5	0.154	-16.5	0.2	151.1	8.35	
16.0	0.803	45.1	2.22	1.291	-60.1	0.159	-23.2	0.224	129.5	9.10	
17.0	0.823	37.2	1.26	1.156	-70.3	0.165	-29.8	0.269	107.3	8.45	
18.0	0.872	31.0	0.27	1.032	-80.2	0.168	-36.6	0.325	88.8	7.88	

**Typical Noise Parameters,  $V_{DS} = 2.7V$ ,  $I_{DS} = 20\text{ mA}$**

Freq GHz	$F_{min}$ dB	$\Gamma_{opt}$ Mag.	$\Gamma_{opt}$ Ang.	$R_{n/50}$	$G_a$ dB
0.5	0.18	0.61	-6.7	0.12	24.89
0.9	0.18	0.55	5.9	0.11	22.72
1.0	0.23	0.49	9.9	0.10	22.68
1.9	0.39	0.43	37.8	0.09	19.18
2.0	0.36	0.42	41.6	0.09	18.98
2.4	0.43	0.37	51.7	0.09	17.83
3.0	0.51	0.29	73.6	0.08	16.69
3.9	0.56	0.26	110.7	0.07	15.19
5.0	0.68	0.28	152.8	0.05	13.79
5.8	0.83	0.33	172.9	0.05	12.91
6.0	0.85	0.33	175.6	0.05	12.73
7.0	0.95	0.37	-162.4	0.06	11.80
8.0	1.06	0.41	-148.8	0.08	11.06
9.0	1.19	0.47	-135.5	0.10	10.47
10.0	1.41	0.46	-119.2	0.17	9.59

**Notes:**

1. The  $F_{min}$  values are based on a set of 16 noise figure measurements made at 16 different impedances using an ATN NP5 test system. From these measurements  $F_{min}$  is calculated. Refer to the noise parameter measurement section for more information.
2. S and noise parameters are measured on a microstrip line made on 0.010 inch thick alumina carrier assembly. The input reference plane is at the end of the gate pad. The output reference plane is at the end of the drain pad.



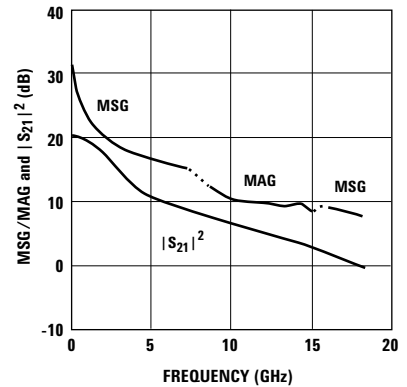
**Figure 31. MSG/MAG and  $|S_{21}|^2$  vs. Frequency at 2.7V, 20 mA.**

**ATF-551M4 Typical Scattering Parameters,  $V_{DS} = 3V, I_{DS} = 10\text{ mA}$**

Freq. GHz	$S_{11}$			$S_{21}$			$S_{12}$		$S_{22}$		MSG/MAG dB
	Mag.	Ang.	dB	Mag.	Ang.	Mag.	Ang.	Mag.	Ang.		
0.1	0.996	-5.9	20.49	10.578	176.0	0.006	86.1	0.835	-2.8	32.46	
0.5	0.957	-28.4	20.05	10.059	158.5	0.027	72.0	0.792	-13.4	25.71	
0.9	0.909	-49.6	19.48	9.420	144.8	0.045	61.5	0.747	-23.5	23.21	
1.0	0.899	-54.6	19.32	9.246	141.6	0.049	59.1	0.730	-25.9	22.76	
1.5	0.836	-78.1	18.32	8.241	126.3	0.065	47.9	0.653	-36.1	21.03	
1.9	0.792	-94.9	17.41	7.424	115.7	0.074	40.3	0.593	-42.7	20.01	
2.0	0.782	-98.8	17.20	7.241	113.2	0.075	38.6	0.578	-44.2	19.85	
2.5	0.740	-116.8	16.07	6.360	101.9	0.082	31.3	0.513	-50.7	18.90	
3.0	0.709	-132.8	14.99	5.616	91.9	0.086	25.3	0.458	-56.0	18.15	
4.0	0.680	-158.5	13.03	4.481	75.1	0.090	16.9	0.378	-64.9	16.97	
5.0	0.675	-178.4	11.33	3.684	60.9	0.091	11.3	0.325	-73.5	16.07	
6.0	0.675	167.8	9.96	3.146	49.1	0.092	8.7	0.287	-79.1	15.34	
7.0	0.676	155.1	8.75	2.738	37.6	0.093	6.6	0.267	-88.4	14.69	
8.0	0.678	144.9	7.77	2.447	26.8	0.095	5.4	0.252	-98.6	12.90	
9.0	0.686	133.8	6.88	2.209	16.0	0.099	4.1	0.242	-110.5	11.73	
10.0	0.682	120.5	6.09	2.015	4.7	0.104	2.1	0.241	-122.9	10.56	
11.0	0.688	107.5	5.37	1.855	-6.3	0.110	0.0	0.247	-135.1	9.88	
12.0	0.694	93.3	4.67	1.711	-17.8	0.118	-3.4	0.256	-146.5	9.26	
13.0	0.711	82.4	3.92	1.571	-28.8	0.127	-6.9	0.250	-159.0	8.76	
14.0	0.746	67.5	3.24	1.452	-40.8	0.137	-12.6	0.240	-176.5	8.90	
15.0	0.753	55.9	2.41	1.320	-52.4	0.146	-18.5	0.246	163.0	7.74	
16.0	0.807	45.8	1.46	1.183	-63.1	0.152	-24.5	0.260	142.0	8.91	
17.0	0.826	37.6	0.48	1.057	-73.7	0.159	-30.8	0.297	119.0	8.23	
18.0	0.874	31.3	-0.53	0.941	-84.1	0.164	-37.5	0.349	98.9	7.59	

**Typical Noise Parameters,  $V_{DS} = 3V, I_{DS} = 10\text{ mA}$**

Freq GHz	$F_{min}$ dB	$\Gamma_{opt}$ Mag.	$\Gamma_{opt}$ Ang.	$R_{n/50}$	$G_a$ dB
0.5	0.23	0.65	-4.3	0.14	23.81
0.9	0.24	0.58	7.4	0.13	21.82
1.0	0.26	0.54	10.7	0.13	21.62
1.9	0.43	0.50	36.2	0.11	18.05
2.0	0.38	0.48	40.4	0.12	17.96
2.4	0.43	0.44	49.8	0.11	16.84
3.0	0.51	0.36	69.2	0.10	15.76
3.9	0.59	0.31	99.4	0.08	14.23
5.0	0.70	0.32	139.3	0.06	12.94
5.8	0.85	0.35	160.3	0.05	12.04
6.0	0.86	0.35	162.3	0.05	11.85
7.0	0.98	0.36	-173.7	0.06	10.99
8.0	1.09	0.41	-158.6	0.07	10.29
9.0	1.23	0.45	-143.7	0.09	9.71
10.0	1.45	0.44	-126.8	0.15	8.88



**Figure 32. MSG/MAG and  $|S_{21}|^2$  vs. Frequency at 3V, 10 mA.**

**Notes:**

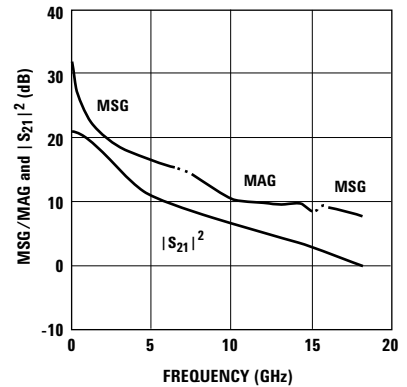
1. The  $F_{min}$  values are based on a set of 16 noise figure measurements made at 16 different impedances using an ATN NP5 test system. From these measurements  $F_{min}$  is calculated. Refer to the noise parameter measurement section for more information.
2. S and noise parameters are measured on a microstrip line made on 0.010 inch thick alumina carrier assembly. The input reference plane is at the end of the gate pad. The output reference plane is at the end of the drain pad.

**ATF-551M4 Typical Scattering Parameters,  $V_{DS} = 3V, I_{DS} = 15\text{ mA}$**

Freq. GHz	$S_{11}$			$S_{21}$			$S_{12}$		$S_{22}$		MSG/MAG dB
	Mag.	Ang.	dB	Mag.	Ang.	Mag.	Ang.	Mag.	Ang.		
0.1	0.995	-6.5	22.02	12.623	175.6	0.005	86.0	0.802	-3.1	34.02	
0.5	0.949	-31.2	21.51	11.900	156.9	0.025	71.0	0.754	-14.6	26.78	
0.9	0.894	-54.1	20.79	10.958	142.3	0.041	60.1	0.700	-25.4	24.27	
1.0	0.882	-59.4	20.59	10.701	138.9	0.045	57.6	0.682	-27.8	23.76	
1.5	0.813	-84.0	19.41	9.341	123.3	0.059	46.7	0.599	-38.1	22.00	
1.9	0.768	-101.2	18.38	8.301	112.7	0.066	39.7	0.537	-44.5	21.00	
2.0	0.758	-105.1	18.14	8.068	110.3	0.067	38.1	0.522	-45.9	20.81	
2.5	0.717	-123.1	16.90	6.996	99.2	0.073	31.6	0.459	-52.0	19.82	
3.0	0.690	-138.7	15.74	6.120	89.7	0.076	26.7	0.407	-56.9	19.06	
4.0	0.668	-163.5	13.68	4.829	73.6	0.080	20.0	0.334	-65.0	17.81	
5.0	0.666	177.5	11.93	3.947	59.9	0.082	15.8	0.286	-73.3	16.82	
6.0	0.668	164.4	10.53	3.363	48.5	0.084	14.2	0.250	-78.4	16.02	
7.0	0.670	152.3	9.31	2.921	37.5	0.087	12.9	0.232	-87.6	14.96	
8.0	0.672	142.4	8.32	2.607	27.0	0.092	11.8	0.218	-97.7	12.99	
9.0	0.681	131.7	7.43	2.351	16.4	0.098	10.4	0.209	-110.0	12.01	
10.0	0.678	118.6	6.62	2.142	5.3	0.104	7.8	0.209	-122.9	10.90	
11.0	0.684	105.8	5.89	1.970	-5.5	0.113	4.9	0.215	-135.4	10.28	
12.0	0.690	91.8	5.19	1.817	-16.8	0.122	0.7	0.226	-147.1	9.70	
13.0	0.707	81.3	4.44	1.667	-27.6	0.132	-3.7	0.221	-160.3	9.23	
14.0	0.744	66.6	3.75	1.540	-39.5	0.142	-10.0	0.211	-179.5	9.62	
15.0	0.751	55.2	2.93	1.401	-50.7	0.151	-16.4	0.218	159.7	8.26	
16.0	0.807	45.3	1.97	1.254	-61.4	0.157	-22.8	0.236	137.8	9.02	
17.0	0.824	37.3	1.01	1.123	-71.9	0.163	-29.5	0.277	114.5	8.38	
18.0	0.874	31.1	0.02	1.002	-82.0	0.167	-36.2	0.330	95.0	7.78	

**Typical Noise Parameters,  $V_{DS} = 3V, I_{DS} = 15\text{ mA}$**

Freq GHz	$F_{min}$ dB	$\Gamma_{opt}$ Mag.	$\Gamma_{opt}$ Ang.	$R_n/50$	$G_a$ dB
0.5	0.18	0.63	-6.3	0.12	24.41
0.9	0.19	0.56	6.8	0.12	22.45
1.0	0.23	0.51	10.0	0.11	22.29
1.9	0.39	0.46	36.5	0.10	18.75
2.0	0.35	0.44	40.8	0.10	18.61
2.4	0.42	0.39	50.1	0.10	17.46
3.0	0.49	0.31	72.5	0.08	16.42
3.9	0.56	0.27	104.4	0.07	14.80
5.0	0.66	0.29	146.9	0.06	13.48
5.8	0.83	0.33	167.4	0.05	12.58
6.0	0.84	0.33	169.0	0.05	12.38
7.0	0.94	0.35	-166.9	0.06	11.49
8.0	1.05	0.40	-152.7	0.07	10.77
9.0	1.19	0.46	-138.6	0.09	10.23
10.0	1.40	0.44	-121.9	0.16	9.32



**Figure 33. MSG/MAG and  $|S_{21}|^2$  vs. Frequency at 3V, 15 mA.**

**Notes:**

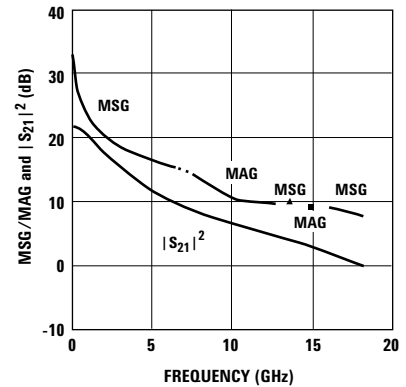
1. The  $F_{min}$  values are based on a set of 16 noise figure measurements made at 16 different impedances using an ATN NP5 test system. From these measurements  $F_{min}$  is calculated. Refer to the noise parameter measurement section for more information.
2. S and noise parameters are measured on a microstrip line made on 0.010 inch thick alumina carrier assembly. The input reference plane is at the end of the gate pad. The output reference plane is at the end of the drain pad.

**ATF-551M4 Typical Scattering Parameters,  $V_{DS} = 3V, I_{DS} = 20\text{ mA}$**

Freq. GHz	$S_{11}$			$S_{21}$			$S_{12}$		$S_{22}$		MSG/MAG dB
	Mag.	Ang.	dB	Mag.	Ang.	Mag.	Ang.	Mag.	Ang.		
0.1	0.995	-6.8	22.91	13.987	175.4	0.005	86.1	0.781	-3.3	34.47	
0.5	0.943	-33.0	22.35	13.101	155.8	0.024	70.5	0.730	-15.2	27.37	
0.9	0.883	-56.9	21.53	11.932	140.7	0.039	59.5	0.672	-26.1	24.86	
1.0	0.870	-62.4	21.30	11.614	137.2	0.042	56.9	0.654	-28.5	24.42	
1.5	0.798	-87.6	20.00	10.004	121.5	0.054	46.3	0.569	-38.5	22.68	
1.9	0.752	-104.9	18.91	8.820	111.0	0.061	39.7	0.506	-44.6	21.60	
2.0	0.743	-108.9	18.64	8.555	108.6	0.062	38.3	0.493	-46.0	21.40	
2.5	0.704	-126.7	17.35	7.368	97.7	0.067	32.4	0.431	-51.6	20.41	
3.0	0.679	-142.1	16.14	6.412	88.4	0.070	28.1	0.383	-56.0	19.62	
4.0	0.660	-166.3	14.03	5.028	72.7	0.074	22.5	0.314	-63.5	18.32	
5.0	0.662	175.3	12.25	4.099	59.4	0.076	19.2	0.270	-71.5	17.32	
6.0	0.664	162.6	10.85	3.488	48.3	0.080	18.3	0.237	-76.2	16.39	
7.0	0.667	150.9	9.62	3.027	37.5	0.084	17.2	0.220	-85.2	14.66	
8.0	0.670	141.3	8.63	2.701	27.2	0.090	16.3	0.207	-95.2	13.18	
9.0	0.679	130.9	7.73	2.435	16.8	0.096	14.6	0.198	-107.6	12.20	
10.0	0.677	118.1	6.92	2.219	5.9	0.104	11.7	0.198	-120.6	11.21	
11.0	0.683	105.4	6.19	2.040	-4.8	0.114	8.4	0.205	-133.4	10.64	
12.0	0.689	91.4	5.49	1.881	-16.0	0.124	3.8	0.216	-145.2	10.10	
13.0	0.705	80.9	4.75	1.727	-26.8	0.134	-1.0	0.210	-158.4	9.62	
14.0	0.742	66.4	4.05	1.594	-38.6	0.145	-7.7	0.199	-178.0	10.41	
15.0	0.751	55.0	3.23	1.451	-49.8	0.153	-14.4	0.207	160.3	8.80	
16.0	0.806	45.1	2.27	1.298	-60.4	0.159	-21.1	0.225	138.1	9.12	
17.0	0.826	37.2	1.32	1.164	-70.8	0.165	-27.9	0.265	114.0	8.48	
18.0	0.874	31.1	0.33	1.039	-80.8	0.170	-34.9	0.320	94.1	7.86	

**Typical Noise Parameters,  $V_{DS} = 3V, I_{DS} = 20\text{ mA}$**

Freq GHz	$F_{min}$ dB	$\Gamma_{opt}$ Mag.	$\Gamma_{opt}$ Ang.	$R_n/50$	$G_a$ dB
0.5	0.17	0.62	-6.2	0.12	24.92
0.9	0.18	0.55	6.0	0.11	22.79
1.0	0.24	0.50	9.5	0.10	22.59
1.9	0.39	0.43	37.5	0.10	19.22
2.0	0.36	0.41	41.2	0.09	19.00
2.4	0.42	0.37	50.9	0.09	17.83
3.0	0.50	0.29	73.6	0.08	16.72
3.9	0.57	0.25	109.4	0.07	15.18
5.0	0.68	0.28	151.6	0.06	13.80
5.8	0.83	0.32	172.5	0.05	12.93
6.0	0.85	0.33	175.6	0.05	12.77
7.0	0.93	0.36	-162.7	0.06	11.84
8.0	1.05	0.41	-149.1	0.08	11.09
9.0	1.19	0.46	-135.5	0.10	10.53
10.0	1.39	0.45	-119.4	0.17	9.64



**Figure 34. MSG/MAG and  $|S_{21}|^2$  vs. Frequency at 3V, 20 mA.**

**Notes:**

1. The  $F_{min}$  values are based on a set of 16 noise figure measurements made at 16 different impedances using an ATN NP5 test system. From these measurements  $F_{min}$  is calculated. Refer to the noise parameter measurement section for more information.
2. S and noise parameters are measured on a microstrip line made on 0.010 inch thick alumina carrier assembly. The input reference plane is at the end of the gate pad. The output reference plane is at the end of the drain pad.

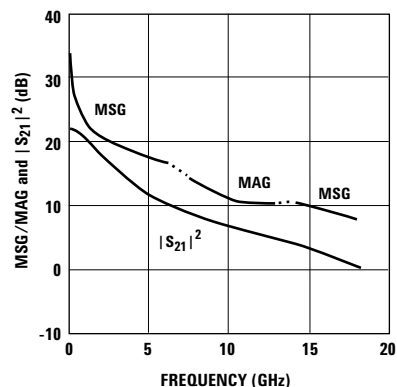


**ATF-551M4 Typical Scattering Parameters,  $V_{DS} = 3V, I_{DS} = 30\text{ mA}$**

Freq. GHz	$S_{11}$			$S_{21}$			$S_{12}$		$S_{22}$		MSG/MAG dB
	Mag.	Ang.	dB	Mag.	Ang.	Mag.	Ang.	Mag.	Ang.		
0.1	0.994	-7.4	23.90	15.662	175.0	0.005	86.1	0.760	-3.4	34.96	
0.5	0.936	-35.3	23.25	14.544	154.5	0.022	69.8	0.705	-15.4	28.20	
0.9	0.870	-60.4	22.32	13.058	138.7	0.035	58.7	0.644	-26.2	25.72	
1.0	0.856	-66.1	22.05	12.665	135.2	0.038	56.2	0.624	-28.5	25.23	
1.5	0.781	-92.0	20.61	10.732	119.4	0.048	46.0	0.539	-37.7	23.49	
1.9	0.736	-109.4	19.44	9.374	108.9	0.054	40.1	0.480	-43.1	22.40	
2.0	0.726	-113.3	19.15	9.072	106.6	0.055	38.8	0.467	-44.2	22.17	
2.5	0.690	-131.0	17.79	7.753	96.0	0.059	33.7	0.410	-49.0	21.19	
3.0	0.668	-146.1	16.54	6.713	86.9	0.062	30.3	0.367	-52.7	20.35	
4.0	0.653	-169.6	14.38	5.234	71.7	0.066	26.1	0.307	-59.2	18.99	
5.0	0.656	172.7	12.58	4.258	58.7	0.069	23.8	0.268	-66.7	17.90	
6.0	0.659	160.5	11.17	3.618	47.9	0.074	23.6	0.238	-70.9	16.89	
7.0	0.663	149.0	9.93	3.138	37.2	0.079	22.9	0.224	-79.8	14.61	
8.0	0.666	139.6	8.94	2.798	27.1	0.086	21.9	0.211	-89.5	13.35	
9.0	0.676	129.3	8.03	2.522	16.8	0.094	20.1	0.203	-101.5	12.55	
10.0	0.674	116.6	7.22	2.296	5.9	0.103	16.9	0.202	-114.5	11.58	
11.0	0.680	104.1	6.48	2.109	-4.6	0.113	13.1	0.208	-127.3	11.01	
12.0	0.688	90.3	5.77	1.944	-15.8	0.124	8.0	0.219	-139.4	10.62	
13.0	0.705	80.1	5.03	1.784	-26.4	0.135	3.0	0.213	-152.3	10.38	
14.0	0.743	65.8	4.34	1.648	-38.0	0.147	-4.1	0.200	-170.8	10.50	
15.0	0.751	54.5	3.53	1.502	-49.2	0.156	-11.1	0.203	166.8	9.84	
16.0	0.806	44.9	2.56	1.343	-59.8	0.162	-18.1	0.218	143.9	9.19	
17.0	0.826	37.0	1.64	1.208	-70.1	0.168	-25.2	0.254	118.4	8.57	
18.0	0.875	31.0	0.67	1.080	-80.2	0.174	-32.4	0.306	97.4	7.93	

**Typical Noise Parameters,  $V_{DS} = 3V, I_{DS} = 30\text{ mA}$**

Freq GHz	$F_{min}$ dB	$\Gamma_{opt}$ Mag.	$\Gamma_{opt}$ Ang.	$R_{n/50}$	$G_a$ dB
0.5	0.16	0.60	-6.2	0.11	25.60
0.9	0.18	0.55	6.4	0.11	23.17
1.0	0.24	0.47	10.1	0.10	23.19
1.9	0.39	0.39	39.1	0.09	19.73
2.0	0.36	0.38	42.7	0.09	19.48
2.4	0.45	0.33	54.2	0.09	18.36
3.0	0.52	0.26	79.0	0.08	17.20
3.9	0.59	0.23	119.0	0.06	15.66
5.0	0.71	0.28	162.1	0.05	14.28
5.8	0.86	0.33	-179.3	0.05	13.39
6.0	0.89	0.33	-176.7	0.05	13.20
7.0	0.99	0.37	-156.1	0.07	12.27
8.0	1.12	0.42	-143.5	0.09	11.50
9.0	1.26	0.48	-130.8	0.12	10.96
10.0	1.50	0.46	-115.1	0.20	10.01



**Figure 35. MSG/MAG and  $|S_{21}|^2$  vs. Frequency at 3V, 30 mA.**

**Notes:**

1. The  $F_{min}$  values are based on a set of 16 noise figure measurements made at 16 different impedances using an ATN NP5 test system. From these measurements  $F_{min}$  is calculated. Refer to the noise parameter measurement section for more information.
2. S and noise parameters are measured on a microstrip line made on 0.010 inch thick alumina carrier assembly. The input reference plane is at the end of the gate pad. The output reference plane is at the end of the drain pad.

## S and Noise Parameter Measurements

The position of the reference planes used for the measurement of both S and Noise Parameter measurements is shown in Figure 36. The reference plane can be described as being at the center of both the gate and drain pads.

S and noise parameters are measured with a 50 ohm microstrip test fixture made with a 0.010" thickness aluminum substrate. Both source pads are connected directly to ground via a 0.010" thickness metal rib which provides a very low inductance path to ground for both source pads. The inductance associated with the addition of printed circuit board plated through holes and source bypass capacitors must be added to the computer circuit simulation to properly model the effect of grounding the source leads in a typical amplifier design.

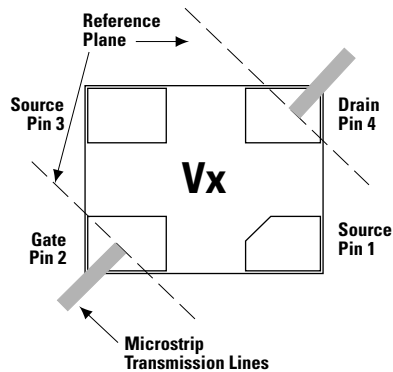


Figure 36. Position of the Reference Planes.

## Noise Parameter Applications Information

The  $F_{min}$  values are based on a set of 16 noise figure measurements made at 16 different impedances using an ATN NP5 test system. From these measurements, a true  $F_{min}$  is calculated.  $F_{min}$  represents the true minimum noise figure of the device when the device is presented with an impedance matching network that transforms the

source impedance, typically  $50\Omega$ , to an impedance represented by the reflection coefficient  $\Gamma_o$ . The designer must design a matching network that will present  $\Gamma_o$  to the device with minimal associated circuit losses. The noise figure of the completed amplifier is equal to the noise figure of the device plus the losses of the matching network preceding the device. The noise figure of the device is equal to  $F_{min}$  only when the device is presented with  $\Gamma_o$ . If the reflection coefficient of the matching network is other than  $\Gamma_o$ , then the noise figure of the device will be greater than  $F_{min}$  based on the following equation.

$$NF = F_{min} + 4 \frac{R_n}{Z_o} \frac{|\Gamma_s - \Gamma_o|^2}{(1 + |\Gamma_o|^2)(1 - |\Gamma_s|^2)}$$

Where  $R_n/Z_o$  is the normalized noise resistance,  $\Gamma_o$  is the optimum reflection coefficient required to produce  $F_{min}$  and  $\Gamma_s$  is the reflection coefficient of the source impedance actually presented to the device.

The losses of the matching networks are non-zero and they will also add to the noise figure of the device creating a higher amplifier noise figure. The losses of the matching networks are related to the Q of the components and associated printed circuit board loss.  $\Gamma_o$  is typically fairly low at higher frequencies and increases as frequency is lowered. Larger gate width devices will typically have a lower  $\Gamma_o$  as compared to narrower gate width devices. Typically for FETs, the higher  $\Gamma_o$  usually infers that an impedance much higher than  $50\Omega$  is required for the device to produce  $F_{min}$ . At VHF frequencies and even lower L Band frequencies, the required impedance can be in the vicinity of several thousand

ohms. Matching to such a high impedance requires very hi-Q components in order to minimize circuit losses. As an example at 900 MHz, when air wound coils ( $Q > 100$ ) are used for matching networks, the loss can still be up to 0.25 dB which will add directly to the noise figure of the device. Using multilayer molded inductors with Qs in the 30 to 50 range results in additional loss over the air wound coil. Losses as high as 0.5 dB or greater add to the typical 0.15 dB  $F_{min}$  of the device creating an amplifier noise figure of nearly 0.65 dB.

## SMT Assembly

The package can be soldered using either lead-bearing or lead-free alloys (higher peak temperatures). Reliable assembly of surface mount components is a complex process that involves many material, process, and equipment factors, including: method of heating (e.g. IR or vapor phase reflow, wave soldering, etc) circuit board material, conductor thickness and pattern, type of solder alloy, and the thermal conductivity and thermal mass of components. Components with a low mass, such as the Minipak 1412 package, will reach solder reflow temperatures faster than those with a greater mass.

The recommended leaded solder reflow time-temperature profile is shown in Figure 37. This profile is representative of an IR reflow type of surface mount assembly process. After ramping up from room temperature, the circuit board with components attached to it (held in place with solder paste) passes through one or more preheat zones. The preheat zones increase the temperature of the board and components to prevent thermal shock and begin evaporating solvents from the solder paste. The reflow zone

briefly elevates the temperature sufficiently to produce a reflow of the solder.

The rates of change of temperature for the ramp-up and cool-down zones are chosen to be low enough to not cause deformation of board or damage to components due to thermal shock. The maximum temperature in the reflow zone ( $T_{max}$ ) should not exceed 235°C for leaded solder.

These parameters are typical for a surface mount assembly process for the ATF-551M4. As a general guideline, the circuit board and components should only be exposed to the minimum temperatures and times the necessary to achieve a uniform reflow of solder.

The recommended lead-free reflow profile is shown in Figure 38.

#### Electrostatic Sensitivity

FETs and RFICs are electrostatic discharge (ESD) sensitive devices. Agilent devices are manufactured using a very robust and reliable PHEMT process, however, permanent damage may occur to these devices if they are subjected to high-energy electrostatic discharges. Electrostatic charges as high as several thousand volts (which readily accumulate on the human body and on test equipment) can discharge without detection and may result in failure or degradation in performance and reliability.

Electronic devices may be subjected to ESD damage in any of the following areas:

- Storage & handling
- Inspection
- Assembly & testing
- In-circuit use

The ATF-551M4 is an ESD Class 1 device. Therefore, proper ESD precautions are recommended when handling, inspecting, testing, and assembling these devices to avoid damage.

Any user-accessible points in wireless equipment (e.g. antenna or battery terminals) provide an opportunity for ESD damage.

For circuit applications in which the ATF-551M4 is used as an input or output stage with close coupling to an external antenna, the device should be protected from high voltage spikes due to human contact with the antenna. A good practice, illustrated in Figure 39, is to place a shunt inductor or RF choke at the antenna connection to protect the receiver and transmitter circuits. It is often advantageous to integrate the RF choke into the design of the diplexer or T/R switch control circuitry.

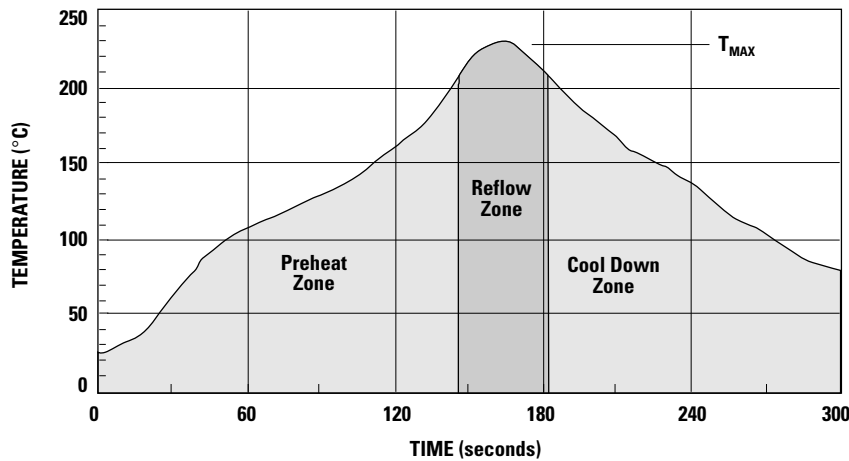


Figure 37. Leaded Solder Reflow Profile.

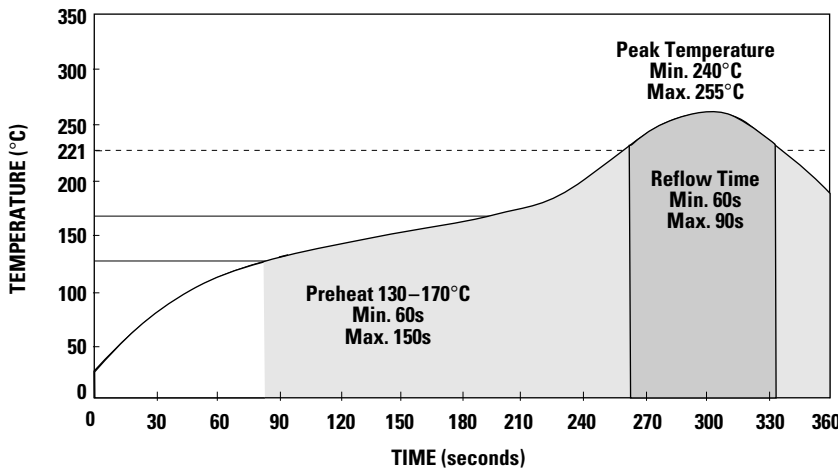


Figure 38. Lead-free Solder Reflow Profile.

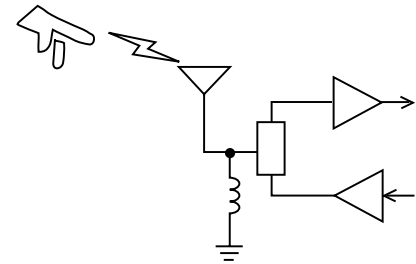


Figure 39. In-circuit ESD Protection.

## ATF-551M4 Applications Information

### Introduction

Agilent Technologies's ATF-551M4 is a low noise enhancement mode PHEMT designed for use in low cost commercial applications in the VHF through 10 GHz frequency range. As opposed to a typical depletion mode PHEMT where the gate must be made negative with respect to the source for proper operation, an enhancement mode PHEMT requires that the gate be made more positive than the source for normal operation. Therefore a negative power supply voltage is not required for an enhancement mode device. Biasing an enhancement mode PHEMT is much like biasing the typical bipolar junction transistor. Instead of a 0.7V base to emitter voltage, the ATF-551M4 enhancement mode PHEMT requires a nominal 0.47V potential between the gate and source for a nominal drain current of 10 mA.

### Matching Networks

The techniques for impedance matching an enhancement mode device are very similar to those for matching a depletion mode device. The only difference is in the method of supplying gate bias. S and Noise Parameters for various bias conditions are listed in this data sheet. The circuit shown in Figure 1 shows a typical LNA circuit normally used for 900 and 1900 MHz applications. Consult the Agilent Technologies web site for application notes covering specific designs and applications. High pass impedance matching networks consisting of L1/C1 and L4/C4 provide the appropriate match for noise figure, gain, S11 and S22. The high pass structure also provides low frequency gain reduction which can be beneficial

from the standpoint of improving out-of-band rejection.

Capacitors C2 and C5 provide a low impedance in-band RF bypass for the matching networks. Resistors R3 and R4 provide a very important low frequency termination for the device. The resistive termination improves low frequency stability. Capacitors C3 and C6 provide the RF bypass for resistors R3 and R4. Their value should be chosen carefully as C3 and C6 also provide a termination for low frequency mixing products. These mixing products are as a result of two or more in-band signals mixing and producing third order in-band distortion products. The low frequency or difference mixing products are terminated by C3 and C6. For best suppression of third order distortion products based on the CDMA 1.25 MHz signal spacing, C3 and C6 should be 0.1 uF in value. Smaller values of capacitance will not suppress the generation of the 1.25 MHz difference signal and as a result will show up as poorer two tone IP3 results.

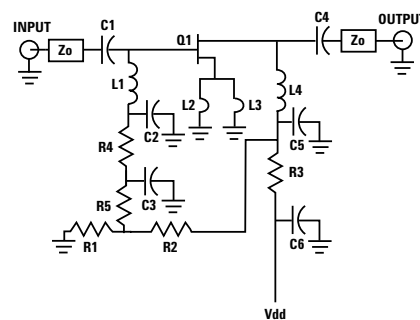


Figure 1. Typical ATF-551M4 LNA with Passive Biasing.

### Bias Networks

One of the major advantages of the enhancement mode technology is that it allows the designer to be able to dc ground the source leads and then merely

apply a positive voltage on the gate to set the desired amount of quiescent drain current  $I_d$ .

Whereas a depletion mode PHEMT pulls maximum drain current when  $V_{gs}=0V$ , an enhancement mode PHEMT pulls only a small amount of leakage current when  $V_{gs}=0V$ . Only when  $V_{gs}$  is increased above  $V_{th}$ , the device threshold voltage, will drain current start to flow. At a  $V_{ds}$  of 2.7V and a nominal  $V_{gs}$  of 0.47V, the drain current  $I_d$  will be approximately 10 mA. The data sheet suggests a minimum and maximum  $V_{gs}$  over which the desired amount of drain current will be achieved. It is also important to note that if the gate terminal is left open circuited, the device will pull some amount of drain current due to leakage current creating a voltage differential between the gate and source terminals.

### Passive Biasing

Passive biasing of the ATF-551M4 is accomplished by the use of a voltage divider consisting of R1 and R2. The voltage for the divider is derived from the drain voltage which provides a form of voltage feedback through the use of R3 to help keep drain current constant. In the case of a typical depletion mode FET, the voltage divider which is normally connected to a negative voltage source is connected to the gate through resistor R4. Additional resistance in the form of R5 (approximately 10K $\Omega$ ) is added to provide current limiting for the gate of enhancement mode devices such as the ATF-551M4. This is especially important when the device is driven to P1dB or Psat.

Resistor R3 is calculated based on desired  $V_{ds}$ ,  $I_{ds}$  and available power supply voltage.

$$R3 = \frac{V_{DD} - V_{ds}}{I_{ds} + I_{BB}} \quad (1)$$

$V_{DD}$  is the power supply voltage.  
 $V_{ds}$  is the device drain to source voltage.

$I_{ds}$  is the desired drain current.  
 $I_{BB}$  is the current flowing through the R1/R2 resistor voltage divider network.

The value of resistors R1 and R2 are calculated with the following formulas.

$$R1 = \frac{V_{gs}}{I_{BB}} \quad (2)$$

$$R2 = \frac{(V_{ds} - V_{gs}) R1}{V_{gs}} \quad (3)$$

#### Example Circuit

$$\begin{aligned} V_{DD} &= 3V \\ V_{ds} &= 2.7V \\ I_{ds} &= 10 \text{ mA} \\ V_{gs} &= 0.47V \end{aligned}$$

Choose  $I_{BB}$  to be at least 10X the maximum expected gate leakage current.  $I_{BB}$  was conservatively chosen to be 0.5 mA for this example. Using equations (1), (2), and (3) the resistors are calculated as follows

$$\begin{aligned} R1 &= 940\Omega \\ R2 &= 4460\Omega \\ R3 &= 28.6\Omega \end{aligned}$$

#### Active Biasing

Active biasing provides a means of keeping the quiescent bias point constant over temperature and constant over lot to lot variations in device dc performance. The advantage of the active biasing of an enhancement mode PHEMT versus a depletion mode PHEMT is that a negative power source is not required. The techniques of active biasing an enhancement mode device are very similar to those used to bias a bipolar junction transistor.

An active bias scheme is shown in Figure 2.

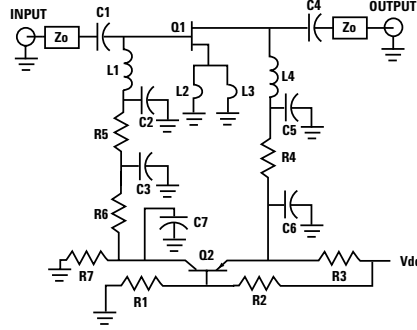


Figure 2. Typical ATF-551M4 LNA with Active Biasing.

R1 and R2 provide a constant voltage source at the base of a PNP transistor at Q2. The constant voltage at the base of Q2 is raised by 0.7 volts at the emitter. The constant emitter voltage plus the regulated  $V_{DD}$  supply are present across resistor R3. Constant voltage across R3 provides a constant current supply for the drain current. Resistors R1 and R2 are used to set the desired  $V_{ds}$ . The combined series value of these resistors also sets the amount of extra current consumed by the bias network. The equations that describe the circuit's operation are as follows.

$$V_E = V_{ds} + (I_{ds} \cdot R4) \quad (1)$$

$$R3 = \frac{V_{DD} - V_E}{I_{ds}} \quad (2)$$

$$V_B = V_E - V_{BE} \quad (3)$$

$$V_B = \frac{R1}{R1 + R2} V_{DD} \quad (4)$$

$$V_{DD} = I_{BB} (R1 + R2) \quad (5)$$

Rearranging equation (4) provides the following formula

$$R2 = \frac{R1 (V_{DD} - V_B)}{V_B} \quad (4A)$$

and rearranging equation (5) provides the follow formula

$$R1 = \frac{V_{DD}}{I_{BB} \left( 1 + \frac{V_{DD} - V_B}{V_B} \right)} \quad (5A)$$

#### Example Circuit

$$\begin{aligned} V_{DD} &= 3V \\ V_{ds} &= 2.7V \\ I_{ds} &= 10 \text{ mA} \\ R4 &= 10\Omega \\ V_{BE} &= 0.7V \end{aligned}$$

Equation (1) calculates the required voltage at the emitter of the PNP transistor based on desired  $V_{ds}$  and  $I_{ds}$  through resistor R4 to be 2.8V. Equation (2) calculates the value of resistor R3 which determines the drain current  $I_{ds}$ . In the example  $R3=18.2\Omega$ . Equation (3) calculates the voltage required at the junction of resistors R1 and R2. This voltage plus the step-up of the base emitter junction determines the regulated  $V_{ds}$ . Equations (4) and (5) are solved simultaneously to determine the value of resistors R1 and R2. In the example  $R1=4200\Omega$  and  $R2 =1800\Omega$ .

R7 is chosen to be 1 k $\Omega$ . This resistor keeps a small amount of current flowing through Q2 to help maintain bias stability. R6 is chosen to be 10 K $\Omega$ . This value of resistance is high enough to limit Q1 gate current in the presence of high RF drive levels as experienced when Q1 is driven to the P1dB gain compression point. C7 provides a low frequency bypass to keep noise from Q2 effecting the operation of Q1. C7 is typically 0.1  $\mu$ F.

#### Maximum Suggested Gate Current

The maximum suggested gate current for the ATF-551M4 is 1 mA. Incorporating resistor R5 in the passive bias network or resistor R6 in the active bias network safely limits gate current to 500  $\mu$ A at P1dB drive levels. In order to minimize component count in the passive biased amplifier circuit, the 3 resistor bias circuit consisting of R1, R2, and R5 can be simplified if desired. R5 can be removed if R1 is replaced with a 5.6K $\Omega$  resistor

and if R2 is replaced with a 27KΩ resistor. This combination should limit gate current to a safe level.

### PCB Layout

A suggested PCB pad print for the miniature, Minipak 1412 package used by the ATF-551M4 is shown in Figure 3.

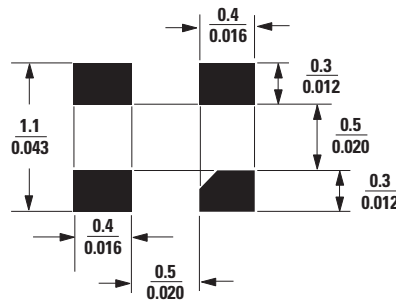
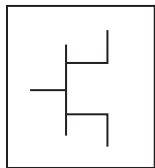


Figure 3. PCB Pad Print for Minipak 1412. Package (mm [inches]).

This pad print provides allowance for package placement by automated assembly equipment without adding excessive parasitics that could impair the high frequency performance of the ATF-551M4. The layout is shown with a footprint of the ATF-551M4 superimposed on the PCB pads for reference.

### ATF-551M4 Die Model



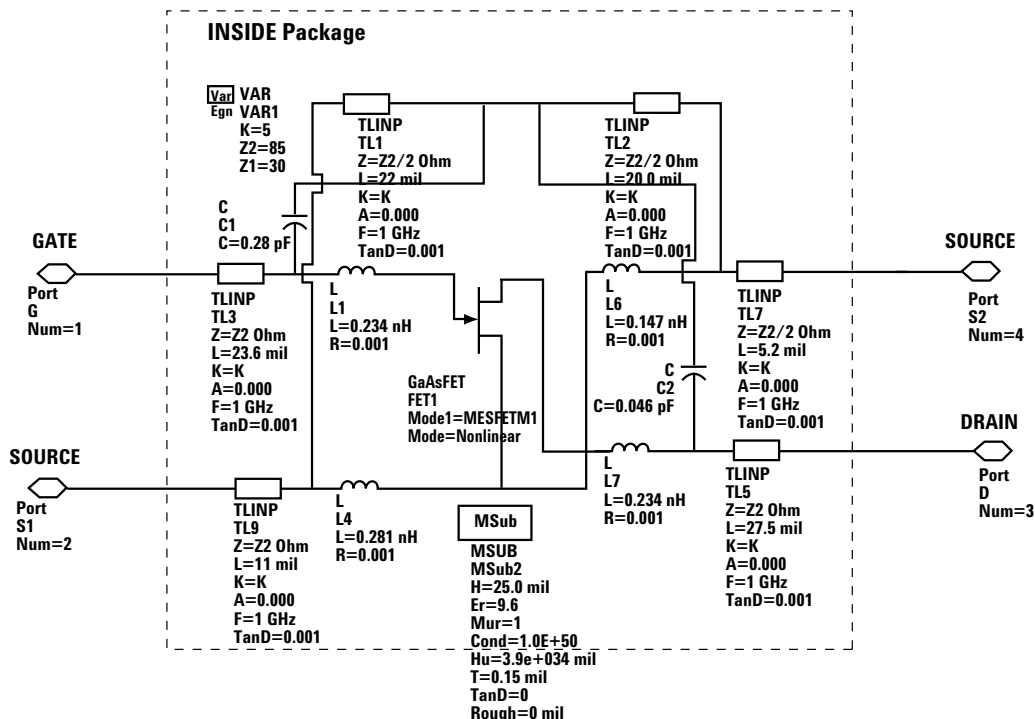
Advanced\_Curtice2\_Model

MESFETM1	Rf=	Crf=0.1 F	N=
NFET=yes	Gscap=2	Gsfwd=	Fnc=1 MHz
PFET=no	Cgs=0.6193 pF	Gsrev=	R=0.08
Vto=0.3	Cgd=0.1435 pF	Gdfwd=	P=0.2
Beta=0.444	Gdcap=2	Gdrev=	C=0.1
Lambda=72e-3	Fc=0.65	R1=	Taumdl=no
Alpha=13	Rgd=0.5 Ohm	R2=	wVgfvwd=
Tau=	Rd=2.025 Ohm	Vbi=0.95	wBvgs=
Tnom=16.85	Rg=1.7 Ohm	Vbr=	wBvgd=
Idstc=	Rs=0.675 Ohm	Vjr=	wBvds=
Ucrit=-0.72	Ld=	Is=	wdsmax=
Vgexp=1.91	Lg=0.094 nH	lr=	wPmax=
Gamds=1e-4	Ls=	lmax=	AllParams=
Vtotc=	Cds=0.100 pF	Xti=	
Betatce=	Rc=390 Ohm	Eg=	
Rgs=0.5 Ohm			

### For Further Information

The information presented here is an introduction to the use of the ATF-551M4 enhancement mode PHEMT. More detailed application circuit information is available from Agilent Technologies. Consult the web page or your local Agilent Technologies sales representative.

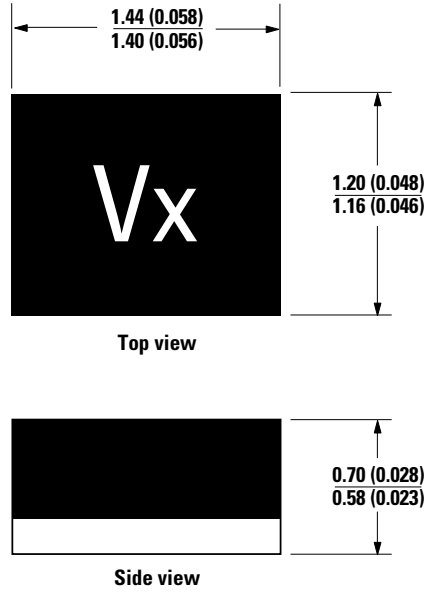
### ATF-551M4 Minipak Model



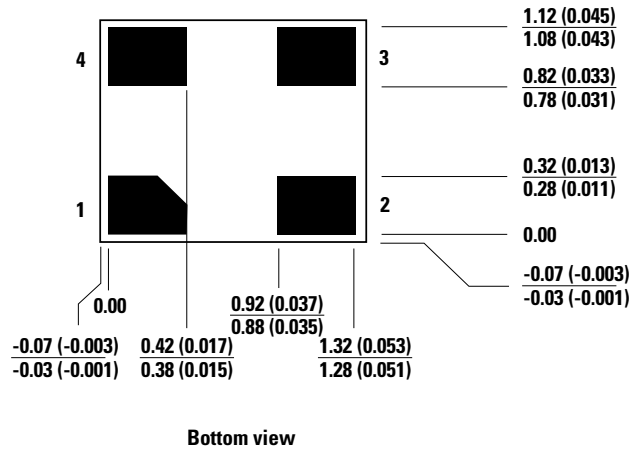
## Ordering Information

Part Number	No. of Devices	Container
ATF-551M4-TR1	3000	7" Reel
ATF-551M4-TR2	10,000	13" Reel
ATF-551M4-BLK	100	antistatic bag

## MiniPak Package Outline Drawing

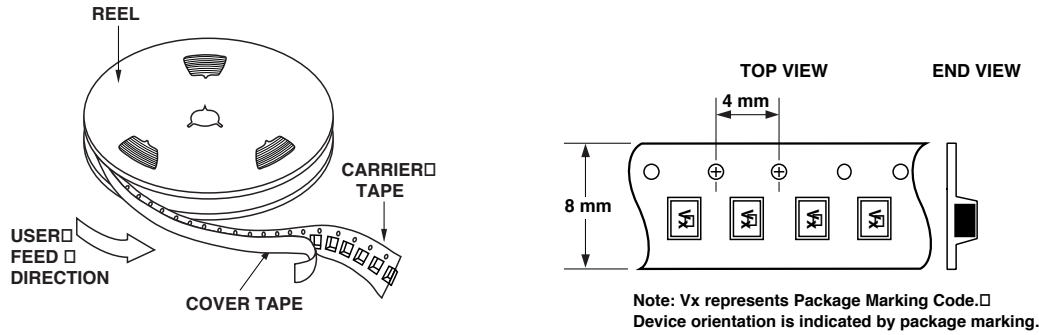


## Solder Pad Dimensions

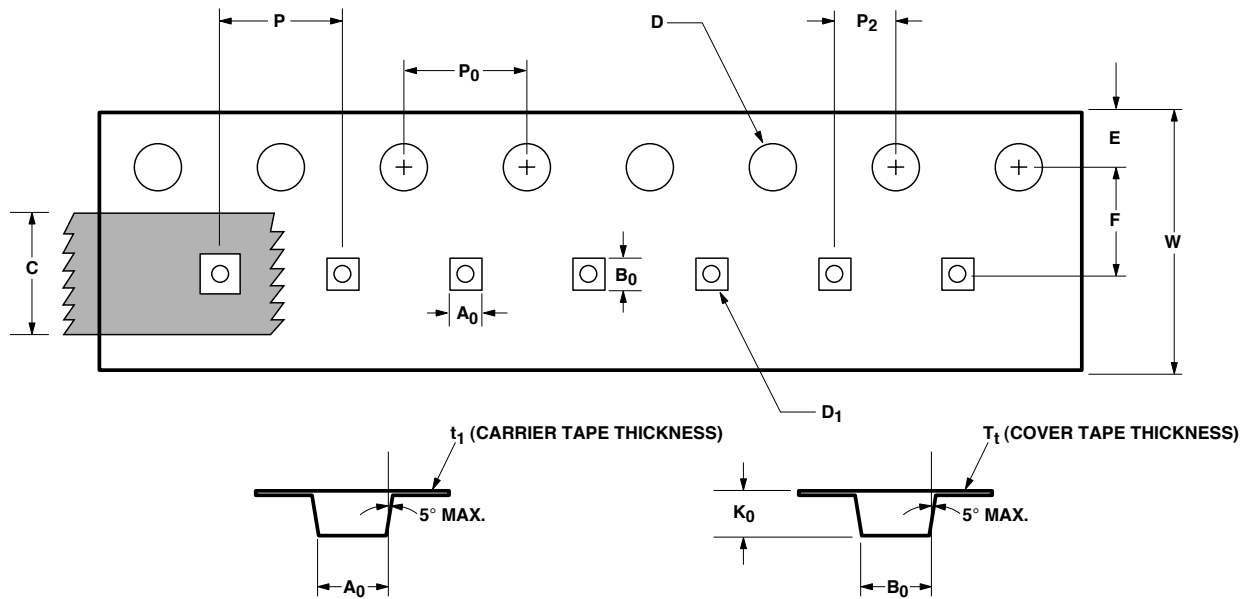


Dimensions are in millimeters (inches)

**Device Orientation for Outline 4T, MiniPak 1412**



**Tape Dimensions**



	DESCRIPTION	SYMBOL	SIZE (mm)	SIZE (INCHES)
CAVITY	LENGTH	A <sub>0</sub>	1.40 ± 0.05	0.055 ± 0.002
	WIDTH	B <sub>0</sub>	1.53 ± 0.05	0.064 ± 0.002
	DEPTH	K <sub>0</sub>	0.80 ± 0.05	0.031 ± 0.002
	PITCH	P	4.00 ± 0.10	0.157 ± 0.004
	BOTTOM HOLE DIAMETER	D <sub>1</sub>	0.80 ± 0.05	0.031 ± 0.002
	PERFORATION	DIAMETER	D	1.50 ± 0.10
PERFORATION	PITCH	P <sub>0</sub>	4.00 ± 0.10	0.157 ± 0.004
	POSITION	E	1.75 ± 0.10	0.069 ± 0.004
	CARRIER TAPE	WIDTH	W	8.00 + 0.30 - 0.10
CARRIER TAPE	THICKNESS	t <sub>1</sub>	0.254 ± 0.02	0.010 ± 0.0008
	COVER TAPE	WIDTH	C	5.40 ± 0.10
COVER TAPE	TAPE THICKNESS	T <sub>t</sub>	0.062 ± 0.001	0.0024 ± 0.00004
DISTANCE	CAVITY TO PERFORATION (WIDTH DIRECTION)	F	3.50 ± 0.05	0.138 ± 0.002
	CAVITY TO PERFORATION (LENGTH DIRECTION)	P <sub>2</sub>	2.00 ± 0.05	0.079 ± 0.002

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