# Fiber-Optic Transmitter and Receiver 

Reliability Data

## Introduction

Agilent Technologies' quality system includes an ongoing reliability monitor program to generate a data base from which this reliability data sheet is published.

## Transmitter Reliability

The HFBR-0400 Series fiber optic transmitters incorporate AIGaAs emitters and double lens optical systems. This design allows the HFBR-14XX transmitters to be driven at a relatively low current level for a specified amount of coupled power into the fiber. Because transmitter forward currents are proportional to failure rates, a low current translates into excellent transmitter reliability. To further improve reliability, Agilent has implemented a proprietary wafer screening technology that identifies dislocations which can lead to the formation of darkline defects (the primary mechanism for transmitter light output failures).

Transmtter reliability data has been calculated using 100 mA forward current and a $100 \%$ duty factor. In many actual use conditions, a $50 \%$ duty factor and lower forward currents are highly probable. When this is true, transmitter reliability will be substantially better. The degree of improvement can be projected by examining the footnotes below the HFBR-14XX data.

## HF BR-0400 Series <br> Transmitters: <br> HFBR-1402, -1412, -1404, -1414 <br> Receivers: <br> HFBR-2402, -2412, -2406, -2416

## Reliability Prediction Model

The reliability prediction model used to project failure rate and mean time to failure (MTTF) at various temperatures shown in the second table assumes an exponential cumulative failure function (constant failure rate). The Arrhenius temperature derating equation is used. Agilent Technologies assumes no failure mechanism change between stress and use conditions. A conservative activation energy of 0.43 eV was used and is derived from MIL-HDBD-217 for hybrid devices. Confidence intervals are based upon the chi-squared prediction method associated with exponential distributions.

## Fiber-Optic Transmitter

## High Temperature Operating Life Test

## A. Demonstrated Performance

| Test | Equivalent Test Condition | Samples | Device Hours | Failures |
| :---: | :--- | :---: | :---: | :---: |
| HTOL | $\mathrm{T}_{\mathrm{A}}=85^{\circ} \mathrm{C}, \mathrm{I}_{\mathrm{F}}=100 \mathrm{~mA}$ | 880 units | 879,500 | 3 |

## B. Failure Criteria

Failure has occurred when the unit fails catastrophically, or when the light output power decreases 3 dB .
C. Failure Rate Prediction for Random Failures (IF @ $100 \mathrm{~mA}, 100 \%$ duty cycle)

|  |  | Point Typical <br> Performance [1] <br> in Time |  | Performance <br> in Time [2] <br> (90\% Confidence) |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Ambient <br> Temperature ( ${ }^{\circ} \mathbf{C}$ ) | Junction <br> Temperature ( ${ }^{\circ} \mathbf{C}$ ) | MTTF [1] <br> (hours) | FITs [3] <br> (/109 Hours) | MTTF [2] <br> (hours) | FITs [3] <br> (/109 Hours) |
| 85 | 100 | 293,000 | 3411 | 131,000 | 7596 |
| 80 | 95 | 352,000 | 2844 | 158,000 | 6334 |
| 75 | 90 | 424,000 | 2360 | 190,000 | 5255 |
| 70 | 85 | 514,000 | 1947 | 231,000 | 4337 |
| 65 | 80 | 626,000 | 1598 | 281,000 | 3560 |
| 60 | 75 | 766,000 | 1305 | 344,000 | 2905 |
| 55 | 70 | 945,000 | 1059 | 424,000 | 2357 |
| 50 | 65 | $1,172,000$ | 854 | 526,000 | 1901 |
| 45 | 60 | $1,462,000$ | 684 | 657,000 | 1523 |
| 40 | 55 | $1,838,000$ | 544 | 825,000 | 1212 |
| 35 | 50 | $2,326,000$ | 430 | $1,044,000$ | 958 |
| 30 | 45 | $2,965,000$ | 337 | $1,331,000$ | 751 |
| 25 | 40 | $3,810,000$ | 263 | $1,711,000$ | 585 |

Notes:

1. The point MTTF (representing an estimate of the mean point MTTF) is the total device hours divided by either the number of failures or unity if there are no failures. 2. $90 \%$ confi dent MTTF and failure rate represent the minimum level of reliability
performance that is expected from $90 \%$ of all samples. This confidence interval is based on the statistics of the distribution of failures. The assumed distribution of failures is exponential. This particular distribution is commonly used in describing
failure rates prior to the onset of wear out. Refer to MIL-STD-690 for details of this methodology.
2. 1 FIT $=1$ failure per 109 device hours.

## Fiber-Optic Link Receiver

## Reliability Data

HFBR-2402
HFBR-2412

## High Temperature Operating Life Test

## A. Demonstrated Performance

| Test | E quivalent Test Condition | Samples | Device Hours | Failures |
| :---: | :--- | :---: | :---: | :---: |
| HTOL | $\mathrm{T}_{\mathrm{A}}=85^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=5.25 \mathrm{~V}$ | 3,960 | $2,370,000$ | 1 |

## B. Failure Criteria

Failure has occurred when the unit
fails catastrophically. One device
failed to switch logic states.
C. Failure Rate Prediction, Receiver ( $\mathrm{V}_{\mathrm{CC}}=5.25 \mathrm{~V}$ )

|  |  | Point Typical <br> Performance [1] <br> in Time |  | Performance <br> in Time [2] <br> (90\% Confidence) |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Ambient <br> Temperature ( ${ }^{\circ} \mathbf{C}$ ) | Junction <br> Temperature ( ${ }^{\circ} \mathbf{C}$ ) | MTTF [1] <br> (hours) | FITs [3] <br> (/109 Hours) | MTTF [2] <br> (hours) | FITs [3] <br> (/109 Hours) |
| 85 | 100 | $2,370,000$ | 421 | 609,000 | 1,640 |
| 80 | 95 | $2,880,000$ | 346 | 742,000 | 1,340 |
| 75 | 90 | $3,530,000$ | 282 | 909,000 | 1,090 |
| 70 | 85 | $4,350,000$ | 229 | $1,120,000$ | 892 |
| 65 | 80 | $5,400,000$ | 184 | $1,390,000$ | 719 |
| 60 | 75 | $6,740,000$ | 148 | $1,730,000$ | 576 |
| 55 | 70 | $8,480,000$ | 117 | $2,180,000$ | 458 |
| 50 | 65 | $10,700,000$ | 93 | $2,750,000$ | 362 |
| 45 | 60 | $13,600,000$ | 73 | $3,510,000$ | 284 |
| 40 | 55 | $17,500,000$ | 56 | $4,520,000$ | 221 |
| 35 | 50 | $22,700,000$ | 43 | $5,850,000$ | 170 |
| 30 | 45 | $29,700,000$ | 33 | $7,650,000$ | 130 |
| 25 | 40 | $39,200,000$ | 25 | $10,000,000$ | 99 |

Notes:

1. The point MTTF (representing an estimate of the mean point MTTF) is the total device hours divided by either the number of failures or unity if there are no failures 2. $90 \%$ confi dent MTTF and failure rate represent the minimum level of reliability
performance that is expected from $90 \%$ of all samples. This confidence interval is based on the statistics of the distribution of failures. The assumed distribution of failures is exponential. This particular distribution is commonly used in describing
useful life failures. Refer to MIL-STD-690 for details of this methodology.
2. $1 \mathrm{FIT}=1$ failure per 109 device hours.

## Fiber-Optic Link Receiver

## Reliability Data

HFBR-2406
HFBR-2416

## High Temperature Operating Life Test

## A. Demonstrated Performance

| Test | E quivalent Test Condition | Samples | Device Hours | Failures |
| :---: | :--- | :---: | :---: | :---: |
| HTOL | $\mathrm{T}_{\mathrm{A}}=85^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=5.25 \mathrm{~V}$ | 2,250 | $2,250,000$ | 0 |

## B. Failure Criteria

Failure has occurred when the unit
fails catastrophically.
C. Failure Rate Prediction, Receiver ( $\mathrm{V}_{\mathrm{CC}}=5.25 \mathrm{~V}$ )

|  |  | Point Typical Performance [1] in Time |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Ambient Temperature ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} \text { Junction } \\ \text { Temperature }\left({ }^{\circ} \mathrm{C}\right) \end{gathered}$ | MTTF [1] (hours) | FITs [3] (/109 Hours) | MTTF [2] (hours) | $\begin{gathered} \text { FITs [3] } \\ (/ 109 \text { Hours }) \end{gathered}$ |
| 85 | 100 | 2,250,000 | 444 | 977,164 | 1023 |
| 80 | 95 | 2,698,516 | 371 | 1,171,953 | 853 |
| 75 | 90 | 3,252,687 | 307 | 1,412,627 | 708 |
| 70 | 85 | 3,941,173 | 254 | 1,711,633 | 584 |
| 65 | 80 | 4,801,432 | 208 | 2,085,240 | 480 |
| 60 | 75 | 5,882,744 | 170 | 2,554,849 | 391 |
| 55 | 70 | 7,250,382 | 138 | 3,148,808 | 318 |
| 50 | 65 | 8,991,407 | 111 | 3,904,927 | 256 |
| 45 | 60 | 11,222,799 | 89 | 4,874,010 | 205 |
| 40 | 55 | 14,102,949 | 71 | 6,124,846 | 163 |
| 35 | 50 | 17,848,023 | 56 | 7,751,315 | 129 |
| 30 | 45 | 22,755,516 | 44 | 9,882,616 | 101 |
| 25 | 40 | 29,238,409 | 34 | 12,698,107 | 79 |

Notes:

1. The point MTTF (representing an estimate of the mean point MTTF) is the total device hours divided by either the number of failures or unity if there are no failures 2. $90 \%$ confi dent MTTF and failure rate represent the minimum level of reliability
performance that is expected from $90 \%$ of all samples. This confidence interval is based on the statistics of the distribution of failures. The assumed distribution of failures is exponential. This particular distribution is commonly used in describing
useful life failures. Refer to MIL-STD-690 for details of this methodology.
2. 1 FIT $=1$ failure per 109 device hours.

## HFBR-0400 Mechanical and Environmental Test Data [1]

| Test Name | MIL-STD-883D Reference | Test Conditions | Units Tested | Total Failed |
| :---: | :---: | :---: | :---: | :---: |
| Temperature Cycle | 1010 | 500 cycles from -55 to $+125^{\circ} \mathrm{C}, 15$ minutes at extremes, 5 minutes transfer. [1] | $\begin{gathered} 2020 \\ \text { HFBR-1414 } \end{gathered}$ | 1 |
|  |  | 500 cycles from -55 to $+125^{\circ} \mathrm{C}, 15$ minutes at extremes, 5 minutes transfer. [1] | $\begin{gathered} 2090 \\ \text { HF BR }-2416 \end{gathered}$ | 0 |
| 85/85 |  | $\mathrm{T}_{\mathrm{A}}=85^{\circ} \mathrm{C}, 85 \%$ relative humidity, No bias, duration $=1,000$ hours. [1] | $\begin{gathered} 2140 \\ \text { HFBR-1414 } \\ \hline \end{gathered}$ | 7 |
|  |  | $\mathrm{T}_{\mathrm{A}}=85^{\circ} \mathrm{C}, 85 \%$ relative humidity, $\mathrm{V}_{\mathrm{CC}}=5$ volts, Duration $=1,000$ hours [1] | $\begin{gathered} 2220 \\ \text { HF BR-2416 } \end{gathered}$ | 6 |
| High Temperature Storage | $1008$ <br> Condition B | $\begin{aligned} & \mathrm{T}_{\mathrm{A}}=125^{\circ} \mathrm{C} \\ & 1000 \text { hours } \end{aligned}$ | 80 | 0 |
| Resistance to Solvents | 2015 | Three 1 minute immersions. Brush after solvent immersion. | 20 | 0 |
| Chemical Resistance | - | 5 minutes in Acetone, Methanol, Freon TF and Boiling Water | 20 | 0 |
| Vibration Variable Frequency | 2007, <br> Condition B | 20 Gmin ., 20 to 2000 Hz . <br> 4, 4 minute cycles each $X, Y$, and $Z$. | 20 | 0 |
| Thermal Shock | $1011$ <br> Condition B | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}, 15$ cycles 5 min. dwell / 10 sec. transfer | 60 | 0 |
| Mechanical Shock | 2002, Condition B | 5 blows each $X 1, X 2, Y 1, Y 2, Z 1, Z 2$ 1500 G, 0.5 msec . pulse. | 60 | 0 |
| Port Wear Test [2] | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 500 connectorings <br> Less than 1 dBm variation | 20 | 0 |
| Connector Side Load [3] | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 1 kg side load Less than 1 dBm variation | 10 | 0 |
| Port Strength [4] | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | $6 \mathrm{~kg}-\mathrm{cm}$ ( 5.21 inch-lbs), no port damage | 10 | 0 |
| Seal-Dye Penetrant (Zyglo) | 1014 <br> Condition D | 45 psi, 10 hours No Leakage into microelectronic cavity | 20 | 0 |
| Solderability | 2003 | $245{ }^{\circ} \mathrm{C}$ | 30 | 0 |
| ESD | Method 3015 | Human body model @ 10,000 V | $\begin{gathered} 5 \\ \text { HFBR-1414 } \\ \hline \end{gathered}$ | 0 |
|  |  | Human body model @ 2,000 V | $\begin{gathered} 5 \\ \text { HFBR- } 2402 \end{gathered}$ | 0 |
|  |  | Human body model @ 1000 V | $\begin{gathered} 5 \\ \text { HF BR-2416 } \end{gathered}$ | 0 |

Notes: See following page.

## Notes:

1. Devices were preconditioned with 10 second, $260^{\circ} \mathrm{C}$ solder dip and 20 cycles, $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$, temperature cycle.
2. Coupled power measurements were maximized before and after stress in determining the 1 dBm variation for SMA HFBR-0400 products. HFBR-0400 ST products do not require this due to the improved coupling design.
3. The Connector Side Load test was only applied to HFBR-0400 SMA products. The Connector Side Load testing required that the housing be held so to prevent the leads from yielding. The load was applied through a SMA connectored fiber optic cable, perpendicular to the port. The product family is designed to limit cable and ferrule damage due to cable loading. The support and active leads should yield before damage to the cable or connector occurs. If extreme mechanical abuse of the cable/ connector is anticipated please contact Agilent's Application Department for suggestions about mechanical strain relief. Due to the spring loaded feature of the ST connector, HFBR-0400 ST products will experience 1 dBm coupled power variation at a side load of less than 1 kg .
4. The Port Strength test was designed to gauge the concerns with hand tightening the connector to the fiber optic port. The limit is set to a level beyond most reasonable hand fastening loading.
5. Package tests are defined as stresses that indicate the environmental strength of the package. Units tested indicate the total number of devices taken from the product family. While not all part numbers have been subjected to each stress, worst case products have been included.
